

**Riverside Energy Resource Center Project  
(Docket No. 04-SPPE-01)  
CURE Data Requests Set 3  
(Nos. 16-59)**

**AIR QUALITY**

**Background**

Under CEQA, the air quality impacts of the Project must be mitigated to the point of insignificance if there is any feasible mitigation. Also, the environmental document prepared for the Project must analyze the environmental impacts of proposed mitigation measures themselves. See CEQA Guidelines §15126(c). The Energy Commission has recognized the importance of this analysis in a number of cases. For example, the importance of understanding the location of offsets the applicant plans to use as mitigation was also revealed in the Los Medanos case, where the staff favored and the Commission required offsets from nearby locations due to the localized impacts of the type of emissions involved with that project. *See* Commission Final Decision of Pittsburg District Energy Facility, August 17, 1999, p. 100. Similarly, in the Tesla case, recognizing the phenomenon of transport pollution (where pollution from one area is largely blown to another area due to wind patterns), the CEC will likely require the applicant to fund pollution reduction programs from the San Joaquin Air Basin, even though the project was being proposed in the Bay Area Air Basin. *See* Revised Presiding Member's Proposal Decision, date online: May 13, 2004, pages 145-175.

**Data Requests**

For each pollutant the project will emit into the air, please identify the following information on any and all offsets procured or to be procured by the applicant:

- 16) The type of pollutant represented by the offset;
- 17) The quantity of each offset;
- 18) The date on which the offset was created or will be created;
- 19) The manner in which the offset was generated or will be generated;
- 20) The expiration date of the offset.

**Response:** The following table includes a summary of NO<sub>x</sub> offsets that have been procured for the project. Offset quantities, issue dates, expiration dates, source facility names and locations, and reasons for generation are identified when such data are available. The NO<sub>x</sub> emission offset credits used for this project were issued by SCAQMD in 1994 to facilities that operate under SCAQMD Regulation XX – Regional Clean Air Incentives Market. Because the credits are instruments of an allocation-based regulatory program, SCAQMD does not track the specific date on which an emission reduction occurs. SCAQMD instead tracks the total inventory of credits in the market for each maturity date

and also tracks emissions as they are reported by each facility. SCAQMD ensures that each facility holds adequate offset credits that are eligible for use in the same period in which emissions occur.

Most NO<sub>x</sub> credits are being provided through facility shutdowns and process modifications that have already taken place, and where generation information is available it is included in the preceding table. Unfortunately, generation data are not always available in the RECLAIM market. The offset program allows credits from various sources to be pooled and sold and held by third parties. While current regulations require more detailed disclosure of source data, transactions that were pooled and sold to third parties prior to 2001 would not have been accompanied by such data. Consequently, generation data such as the reason for credit availability or the date on which facility operations changed may not be available for credits being sold today that were previously held by third parties. Cantor-Fitzgerald staff are working with SCAQMD staff in an attempt to identify potential sources of credits that were pooled in the past and that are now part of the credits to be used to offset commissioning operations. As additional information becomes available, it will be shared with CEC.

All other offsets will be provided through SCAQMD's reserve accounts. SCAQMD will present offsets from its reserve accounts to offset increases in SO<sub>x</sub>, CO, VOCs and PM10. SCAQMD is independently submitting a letter to CEC clarifying the structure and validity of its offset program and the credits that will be used for this project. SCAQMD will provide offsets in accordance with the 30-day emissions averages reflected in Table 6.1-23 of the SPPE application report. SCAQMD will offset these emission increases at a ratio of at least 1.0:1.

It is important to note, however, that the absence of generation and other source data does not invalidate the offsets being used for the RERC project. All offsets are offered in full compliance with new source review regulations affecting facilities in the South Coast Air Basin. SCAQMD's method of issuing, tracking and applying offset credits to new sources has been approved by the SCAQMD Governing Board, CARB and US EPA with careful scrutiny of the offset program's effect on regional attainment and maintenance of ambient air quality standards.

#### **RERC NO<sub>x</sub> Offset Credits**

<b>Amount of NO<sub>x</sub> Emission Offsets</b>	<b>Issue Date</b>	<b>Expiration Date</b>	<b>Source</b>	<b>Generation</b>
9,500 lb Inland	1/1/05 and every year after	12/31/05 and every year after	Intermetro Industries 9393 Arrow Route Rancho Cucamonga,	Facility Shutdown – 3/30/04

			CA Facility 5830 (909) 987-4731	
4,000 lb Inland	7/1/05 and every year after	6/30/06 and every year after	Pomona Paper Co. 1404 W. Holt Ave. Pomona, CA Facility 117151	Facility Shutdown – 10/30/02
2,000 lb Coastal	1/1/05 and every year after	12/31/05 and every year after	West Newport Oil 1080 W. 17 <sup>th</sup> Costa Mesa, CA. Facility 42775 (949) 631-1100	Process Change – Complete
4,846 lb Coastal	7/1/05 and every year after	6/30/06 and every year after	Mission Dye 905 E. 8 <sup>th</sup> St. Los Angeles, CA 90021 (213) 236-9780	Facility Shutdown – Complete
1,000 lb Coastal	1/1/05	12/31/05	Purchased through Calpine – source is being investigated but credits were previously pooled and transferred in a blind auction.	Reason for generation is being investigated but credits were previously pooled and transferred in a blind auction.
18,500 lb Coastal	1/1/05	12/31/05	Purchased through Calpine – source is being investigated but credits were previously pooled and transferred in a blind auction.	Reason for generation is being investigated but credits were previously pooled and transferred in a blind auction.

## LAND USE

### **Background**

The maps in the Application are inconsistent and incomplete. The boundaries of the Project site are different on the various maps included in the Application. See, for example, the Zoning Classification figure, following page 112; Fig. 6.7-1; Fig. 6.7-2; and Drawing C1-2, following page 232. Similarly, the Zoning Classification map following page 112 shows that a trail touches the northwest and northeast corners of the Project site. The USGS 7-1/2 minute quad map for the site, Riverside West, also suggests that a trail borders these two corners. However, other maps suggest that the trail is more distant from the project site.

### **Data Requests**

- 21) Please clarify which boundary accurately reflects the proposed plant site.
- 22) Please prepare a map that precisely locates and labels both the recreational trail and the Project site.

**Response:** The attached Map 1 accurately identifies the proposed plant site boundary and the recreational trail.

## **NOISE**

### **Background**

The Application indicates that 25-hour, long-term noise data were collected at three locations at microphone heights of 5 feet and 15 feet. The Application indicates that the data is included in Appendix 6.7-A. (Application, p. 201.) A summary of the data for one site, LY-1, at the 5-foot elevation, is included in Appendix 6.7-A. However, the data for LT-1 at 15 feet and for the other two sites is not.

### **Data Requests**

- 23) Please provide a summary of the noise data collected at LT-1 at 15 feet and at LT- and LT-3 for both 5 feet and 15 feet elevations, comparable to that provided for LT-1 in Appendix 6.7-A.

**Response:** These are provided in Attachment Noise-1.

- 24) Please provide an electronic copy of the raw noise data in ASCII format collected at each station, as downloaded from the Larson Davis 820 SLM.

**Response:** These are provided in Attachment Noise-6.

### **Background**

The Application indicates that short-term noise data were collected at 12 locations and that these measurements are provided in Appendix 6.7-A and summarized in Table 6.7-2. (Ap., p. 201.) However, Appendix 6.7-A does not contain any support for the measurements summarized in Table 6.7-2. Further, Table 6.7-2 is marked "DRAFT."

### **Data Requests**

- 25) Please provide the supporting data for all short-term noise measurements that was omitted from Appendix 6.7-A.

**Response:** These are provided in Attachment Noise-2.

- 26) Please provide an electronic copy of the raw noise data in ASCII format collected at each short-term station, as downloaded from the Larson Davis Model 712 SLM.

**Response:** The short-term measurement data was not downloaded to a computer file, but was written down onto data sheets at the end of each measurement. These are provided in Attachment Noise-2.

- 27) Please provide a final copy of Table 6.7-2.

**Response:** This is provided in Attachment Noise-3.

### **Background**

The nearest acknowledged sensitive receptors are hikers on the recreational trail and noise monitoring site ST-5, located some 690 feet from the acoustic center of the Project site. The noise study collected 25 hours of noise data at the residential sensitive receptors, which are much more distant, but not along the trail. Only 20 minutes of noise data were collected at ST-5, starting at 6 PM on 3/17/04, a Wednesday. (Application, Table 6.7-2.) This is likely not the quietest period that would be experienced by hikers. The noise analysis should have collected 25 hours of data at ST-5 due to its proximity to the site and noise sensitive nature, particularly in the early morning hours.

### **Data Requests**

- 28) Please provide 25-hours of noise data at ST-5 for a Sunday.

**Response:** The data already obtained for ST-5 at 2:12 PM on 3/17/04 (this is the correct time, which differs from that in the data request) provides a representative set of data upon which to evaluate this issue. This is because the primary noise source affecting ST-5, the existing water treatment facility just to the southwest of the position, was operating during the measurement. It is not anticipated that the noise level at ST-5 would be significantly lower than that measured on 3/17/04 unless there was a significant change to the operation at the water treatment facility. Therefore, it is not considered necessary to obtain a 25-hour measurement at this location.

## **Background**

The noise impact analysis is based on CEC significance thresholds summarized in Table 6.7-4. The CEC thresholds are calculated by adding 5 dB to the measured CNEL and Leq. However, the measured CNELs and Leqs reported in Table 6.7-4 are inconsistent with summary data presented in Table 6.7-1. Further, the procedure used to calculate these thresholds appears to be inconsistent with those used in other siting cases. The CEC normally requires that a plant not increase noise levels by more than 5 dBA above existing background measurements, or the most stringent absolute noise level required by any applicable LORS. The CEC's noise significance criterion is calculated by adding 5 dB to the lowest L90 based on 25 hours of data, not to the CNEL or the Leq. The noise significance thresholds would be much lower, and the noise impacts significant, if the lowest L90 had been used to calculate noise significance thresholds. For example, the significance threshold for the recreational trail would have been 45 dBA, rather than 51 dBA.

## **Data Requests**

- 29) Please reconcile the difference between the CNEL and Leq values reported in Table 6.7-4 and those summarized in Table 6.7-1. If the information in Table 6.7-1 represents an average, please provide supporting calculations and identify all assumptions that your calculations are based on.

**Response:** There is no difference between the CNEL values reported in Tables 6.7-4 and 6.7-1. Comparing the two tables, it can be seen that the CNELs measured at second floor receptors were used to develop the CEC impact criteria thresholds used in Table 6.7-4. This is because the second floor receptors will experience the greatest potential impact from the operation of the RERC since they will be least protected by existing barriers. As for the Leq values, Table 6.7-1 provides the 25-hour Leq's, as required by the CEC. Table 6.7-4 provides the lowest measured Leq at each receptor. By comparing the two tables, it can be seen that this approach provides a much more conservative assessment of the project's impact than if a 25-hour Leq was used. The supporting data for Tables 6.7-1 and 6.7-4 are provided in Attachments Noise-1 and Noise-2.

- 30) Please revise Table 6.7-4 to calculate noise significance thresholds based on lowest measured L90, using 25 hours of data for each sensitive receptor.

**Response:** Table 6.7-4 is based on the CNEL and Leq metrics used by the County of Riverside, which is where the nearest noise-sensitive receptors to the project (i.e., the residences to the north) are located. Neither the City nor the County of Riverside uses the L90 metric; therefore, its use to assess the impact of the project is not considered appropriate.

- 31) Please revise the operational noise impact analysis summarized in Figure 6.7-2 and Table 6.7-6 to use the revised significance thresholds.

**Response:** As indicated in the response to Data Request #30, the significance thresholds used in the analysis are considered appropriate. Therefore, it is not necessary to revise Figure 6.7-2 or Table 6.7-6.

- 32) Please revise the construction noise impact analysis in Table 6.7-5 to use the revised significance threshold.

**Response:** As indicated in the response to Data Request #30, the significance thresholds used in the analysis are considered appropriate. Therefore, it is not necessary to revise Table 6.7-5.

### **Background**

The noise analysis concludes that noise impacts are significant if they result in a 5 dB increase above existing noise levels during either construction or operation. (Application, p. 203.) The results of the operational analysis, summarized in Figure 6.7-2, appears to show that the 5 dB noise contour intersects the recreational trail. An increase of 5 dB or more is normally a significant impact.

### **Data Request**

- 33) Please revise Figure 6.7-2 to label the red contour and the recreational trail to clarify what is depicted.

**Response:** The noise contour in Figure 6.7-2 approaches, but does not intersect, the recreational trail. Figure 6.7-2 has been revised to label the red contour and the recreational trail. It is included in this response as Attachment Noise-4.

- 34) Please explain why a 5 dB increase in noise levels during Project operation on or near the recreational trail does not constitute a significant noise impact.

**Response:** The impact is not considered to be significant because of the short-term duration of the exposure. Residential properties are considered to be noise-sensitive because it is assumed that the residents can, and will, be on the property up to 24 hours a day. If a resident is exposed to a 5 dB increase in noise level as a result of the project, his or her exposure can last for however long the RERC is operating. This is quite different from a hiker on a recreational trail who is only exposed to noise from the RERC for the few minutes it takes him or her to pass by the project site.

- 35) The test indicates that Figure 6.7-2 shows the area “where there is a potential increase of 5 dB or more over existing noise levels during normal plant operation.” (Application, p. 204.) Please disclose the “existing noise level” used to estimate this contour.

**Response:** The existing noise levels are found in Table 6.7-2. Referring to the table, the existing Leq at ST-5 is 46 dB(A).

- 36) Please provide an electronic file that contains the detailed calculations used to generate the 5 dB noise contour on Figure 6.7-2.

**Response:** The electronic file is proprietary. However, the calculations of project noise levels are included in this response as Attachment Noise-5.

- 37) Please explain why Table 6.7-6 shows a 0 dB increase on the recreational trail, location ST-5, while Figure 6.7-2 shows a 5 dB increase.

**Response:** Table 6.7-6 does not show changes in noise level. Rather, the last column, labeled “CEC”, indicates by how many decibels the project noise levels are below the CEC significance threshold.

### **Background**

The results of the operational noise analysis, summarized in Table 6.7-6, suggests that noise levels would increase by 5 dB at LT-2, ST-1, ST-3, ST-4, ST-10, and ST-12. An increase of 5 dB or more is normally a significant impact.

### **Data Requests**

- 38) Please explain why the 5 dB increase in operational noise levels at LT-2, ST-1, ST-3, ST-4, ST-10, and ST-12 are not significant.

**Response:** Table 6.7-6 does not show changes in noise level. Rather, the last column, labeled “CEC”, indicates by how many decibels the project noise levels are below the CEC significance threshold.

- 39) Please provide an electronic file that contains the detailed calculations that support the column labeled “CEC” in Table 6.7-6.



**Response:** The electronic file is proprietary. However, the calculations of project noise levels are included in this response as Attachment Noise-5.

### **Background**

The results of the construction noise analysis, summarized in Table 6.7-5, indicates that Project construction will increase noise levels along the recreational trail north of the site by 5 dB. An increase of 5 dB or more is normally a significant impact.

### **Data Requests**

- 40) Please explain why noise impacts along the recreational trail during construction are not significant.

**Response:** The impact is not considered to be significant because of the short-term duration of the exposure. Residential properties are considered to be noise-sensitive because it is assumed that the residents can, and will, be on the property up to 24 hours a day. If a resident is exposed to a 5 dB increase in noise level as a result of the project's construction, his or her exposure can last for however long the construction lasts. This is quite different from a hiker on a recreational trail who is only exposed to construction noise for the few minutes it takes him or her to pass by the project site.

### **Background**

The construction noise impact analysis is summarized in Table 6.7.5. The test briefly explains how the analysis was performed, but does not provide any supporting calculations or sufficient detail to replicate the analysis. The assumptions about the number of pieces of equipment that would be operating and load appear to conflict with assumptions used in the construction emission analysis in Appendix 6.1D.

### **Data Requests**

- 41) Please provide an electronic file that contains the detailed calculations that support the construction noise impact analysis in Table 6.7-5.

**Response:** The calculation procedure is summarized as follows: A conservative assessment of construction noise was obtained by assuming that all of the equipment identified in Table 6.7-7 would be operating simultaneously. Adding together the noise levels provided in the table yields a combined maximum noise level of 94.5 dB(A) at 50 feet. [The Application identifies a combined maximum noise level of 89 dB(A), but this is a typographical error.] Note that this is the *maximum* noise level generated by all of the equipment operating simultaneously, not the *average* (Leq) noise level of the equipment. The average (Leq) for the construction noise is conservatively estimated by assuming a 50% duty cycle, i.e.,

that the equipment will be generating its maximum noise level during 50% of its operating time. With a 50% duty cycle, the combined noise level is reduced by 3 dB [ $10 \cdot \log(50/100) = -3$  dB]. Thus, the combined Leq for the construction equipment is conservatively estimated to be 91.5 dB(A) [ $94.5 - 3 = 91.5$  dB(A)] at 50 feet. Using this base value, corrections for attenuation due to distance, air absorption and barrier effects are applied to derive the estimated construction noise levels identified in Table 6.7-5. This is illustrated as follows:

Parameter	LT-1	LT-2	LT-3	Rec. Trail
Base Noise Level	91.5 dB(A)	91.5 dB(A)	91.5 dB(A)	91.5 dB(A)
Distance Attenuation <sup>1</sup> (distance)	-35.2 dB (2,870')	-38.3 dB (4,130')	-38.5 dB (4,200')	-24 dB (790')
Air Absorption <sup>2</sup>	-8.1 dB	-8.1 dB	-8.1 dB	-0 dB
Barrier Attenuation <sup>3</sup>	-0 dB	-0 dB	-0 dB	-17.5 dB
Construction Noise Level <sup>4</sup>	48 dB(A)	45 dB(A)	45 dB(A)	50 dB(A)

Notes:

1. Based on inverse square law:  $\text{attenuation} = 20 \cdot \log(50/\text{distance})$ .
2. The attenuation due to air absorption increases with distance. Therefore, the attenuation at receptors LT-2 and LT-3 is greater than at receptor LT-1. However, to be conservative, the same attenuation calculated at receptor LT-1 has been used at receptors LT-2 and LT-3. Refer to Attachment Noise-5 for the calculation of air absorption attenuation. No attenuation for air absorption has been assumed at the recreational trail in order to provide a conservative assessment.
3. Refer to Attachment Noise-5 for the barrier attenuation factors used at the recreational trail. No barrier attenuation has been assumed for receptors LT-1 through LT-3 in order to provide a conservative assessment.
4. Obtained by adding together the base noise level, distance attenuation, air absorption and barrier attenuation.

- 42) Will pile drivers be used to construct the project? If no, please explain why not. If yes, please identify the type of pile driver, the number that will be operating at any one time, and their operating schedule.

**Response:** Pile drivers will not be used during construction, as piled foundations are not required. This conclusion is supported by the geotechnical analysis.

### **Background**

A small Power Plant Exemption (“SPPE”) requires that a project will not have any adverse impacts and that all potentially significant environmental impacts will be mitigated to the point of significance. The noise analysis acknowledges that the Project would result in a significant noise impact that cannot be fully mitigated. (Application, p. 205.)

### **Data Requests**

- 43) Please explain why, given this impact, that you believe the Project qualifies for a SPPE.

**Response:** A significant impact will only occur if blasting is required to remove some large boulders during the project's construction. There is no available technology that can be used to completely eliminate this impact. However, the state-of-the-art technology recommended in the Application will be used to reduce the blasting noise to the lowest levels that are technically feasible. Therefore, the Project qualifies for an SPPE.

### **Background**

The last 3,000 feet of the transmission line will be located within about 40 feet of residential property. (Application, p. 206.) The Application did not evaluate the impact of constructing the transmission line on these residential properties, but instead concluded that the activities would be temporary and would not generate any noise. (Application, p. 206.)

### **Data Requests**

- 44) Please provide a quantitative analysis of the impact of transmission line construction on adjacent residential properties.

**Response:** The level of analysis provided in the Application is consistent with that approved by the CEC on other Applications, and is appropriate for the extremely short-term duration (on the order of a few days) of noise exposure that will be experienced by the residents in the vicinity of the construction area.

### **Background**

The Hidden Valley Wildlife Area is immediately north of the plant site. (Application, p. 118, 131.) This area contains wetlands and a riparian corridor and supports a wealth of sensitive species and habitats, including the largest population of an endangered bird species. The Application did not evaluate the impact of noise on wildlife.

### **Data Requests**

- 45) Please provide an analysis of the impact of noise on wildlife in the Hidden Valley Wildlife Area.

**Response:** Because the Hidden Valley Wildlife area is located approximately one mile west of the project site, an analysis of potential noise impacts is not

necessary. The attached Map 2 shows the location of the Hidden Valley Wildlife area in relation to the proposed plant site.

## **WATER RESOURCES**

### **Background**

The Zoning Classification figure following page 112 in the Application shows a well on the western property boundary. This same well is shown on the USGS quad for Riverside West. The Application does not discuss this well.

### **Data Requests**

- 46) Please indicate whether this well is currently in use and if so, whether Project construction and operation will disturb it.

**Response:** The well is not used and will not be disturbed.

### **Background**

The Project's northern boundary abuts the 100-year floodplain boundary. The Application states, with no analysis, that the Project would not be affected by flooding. (Application, p. 327.) The site is characterized as being enclosed by a berm along its northern, eastern, and southern edges. This "berm" was apparently created by excavating fill from the Project site, lowering the Project site compared to the surround land area. (Application, p. 9.) The Application does not indicate whether the "berm" would protect the site from flooding.

### **Data Requests**

- 47) Does the conclusion that flooding would not be significant rely on the presence of the berms?

**Response:** No. The conclusion that flooding would not be significant is based on the fact that the proposed site is not within the designated 100 year floodplain of the Santa Ana River and is elevated above the base flood elevation.

- 48) Please provide an engineering drawing that shows the dimensions of the berms relative to the surrounding land area.

**Response:** The berms are not engineered features. On the north and east faces of the berms, these are pre-existing natural faces. The south and west faces of the berms were created when the hill was removed to cap a landfill thus creating the current site.

- 49) Are the site berms designed to withstand a 100-year flood? If yes, please provide design criteria and supporting geotechnical analyses.

**Response:** As stated in 48, the berms are not engineered. However based on seeing them, they are significant features and can reasonably be expected to be unaffected by a 100 year storm.

### **Background**

Reclaimed water from the City's Water Quality Control Plant is used to support the Hidden Valley Wildlife Area wetlands just north of the Project site. (Application, p. 131.) The Application does not evaluate the impact on these wetlands of diverting a portion of the water currently routed to the wetlands.

### **Data Requests**

- 50) Please evaluate the water quality, water supply, and biological impacts of reducing the flow of reclaimed water to these wetlands.

**Response:** Only a portion of the reclaimed water from the Water Quality Control Plant (WQCP) is supplied to the wetlands. The WQCP has stated that the relatively small amount of water that will be supplied to the RERC will have no impact on those deliveries.

### **Background**

The Project would use reclaimed water from the City's Water Quality Control Plant. The Application identifies the major constituents in this water supply but does not identify the organics or metals, such as arsenic, mercury, cadmium and lead. (Application, Table 2.7-1, p. 20.) The reclaimed water will be injected into the turbine combustors to control NOx or used in the cooling tower. Metals and other contaminants present in the reclaimed water will be emitted at the turbine exhaust stack and from the cooling towers, potentially adversely impacting wildlife in the nearby Hidden Valley Wildlife Area or nearby residents and workers.

### **Data Requests**

- 51) Please provide complete chemical characterization data for the reclaimed water, including trace organics and metals.

**Response:** Please see Attachment Water 1.

### **Background**

The Process Flow Diagram following page 20 indicates that water use would generate 856 lb / day of solid wastes. (Application, Drawing M2-1.) The Application does not divulge the source or composition of this stream.

### **Data Requests**

- 52) Please provide the chemical and physical composition of the solid waste stream, including moisture content, organics and metals.

**Response: COMPOSITION OF SLURRY (WITHOUT FILTER PRESS)**  
Slurry discharge will be approximately 0.4 gpm and will contain 50% total solids. Out of the total solids 10% will be suspended while 40% will be dissolved. In the table below the top three will be suspended while the remaining will be dissolved in the slurry discharge.

	wt%
SiO <sub>2</sub>	0.61
CaCO <sub>3</sub>	0.10
CaSO <sub>4</sub>	9.32
Na <sub>2</sub> SO <sub>4</sub>	4.54
MgSO <sub>4</sub>	0.00
K <sub>2</sub> SO <sub>4</sub>	0.00
NaCl	33.06
MgCl <sub>2</sub>	1.91
KCl	0.00
CaCl <sub>2</sub>	0.00
Mg(NO <sub>3</sub> ) <sub>2</sub>	0.41
KNO <sub>3</sub>	0.00

Other trace elements in the feed water will be concentrated approximately 700 times before they escape with the slurry. But in terms of %, these constituents in the overall slurry will be minimal.

- 53) Please indicate whether this waste stream would be hazardous, state the basis for your conclusion and present all calculations and chemical analyses that support your answer.

**Response:** Please see response 52.

- 54) Please reveal the disposition of this waste stream including:

- 55) whether it will be stored in open ponds or closed containers on site;

**Response:** The waste will be stored in closed containers.

- 56) the number and type of trucks and other equipment that will be used to handle and transport the waste;

**Response:** The waste will be hauled using appropriate trucks or other equipment in compliance with all applicable LORS.

- 57) identity of landfill where the waste will be disposed.

**Response:** Please see the applicant's response to CEC Data Request #71.

## **BIOLOGY**

### **Background**

Sensitive biological species are present in the Hidden Valley Wildlife Area, immediately north of the Project. The public health section of the Application deals only with impacts to humans. The biological resources section does not consider the impact of toxic emissions on wildlife. The standards and protocols for ecological risk assessments are well established and widely used both at the federal and state levels. EPA has issued guidance documents for this purpose. *See* Guidance for Ecological Risk Assessments, February 1992 (EPA/630R-92-001.) Similarly, the State of California has such guidance in place. *See* Guidance for Ecological Risk Assessment at Hazardous Waste Sites and Permitted Facilities, July 4, 1996, Department of Toxic Substances and Control.<sup>1</sup> The potential environmental impacts of the Project – located next to a series – cannot be evaluated without an assessment of the toxic emissions' impacts on these species and their habitat and the development of appropriate mitigation.

### **Data Requests**

- 58) Please prepare an analysis of the impacts of toxic emissions during Project construction and operation on the wildlife that uses the Hidden Valley Wildlife Area.

**Response:** The Hidden Valley Wildlife Area is located approximately 1 mile due west of the project site. We do not believe there will be any significant impacts to the wildlife area. The attached Map 2 shows the location of the Hidden Valley Wildlife area in relation to the proposed plant site.



## **SOCIOECONOMICS**

### **Background**

The Hidden Valley Wildlife Area and associated trail system is located immediately north of the Project. The Application does not contain an analysis of the impact of Project construction and operation on recreation in this Area. The analysis of the Project's visual and noise impacts does not constitute an evaluation of this broader impact on recreation. It is clear that such impacts must be specifically considered under CEQA. This is a major deficiency in the Application which must be corrected.

### **Data Requests**

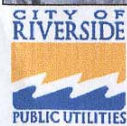
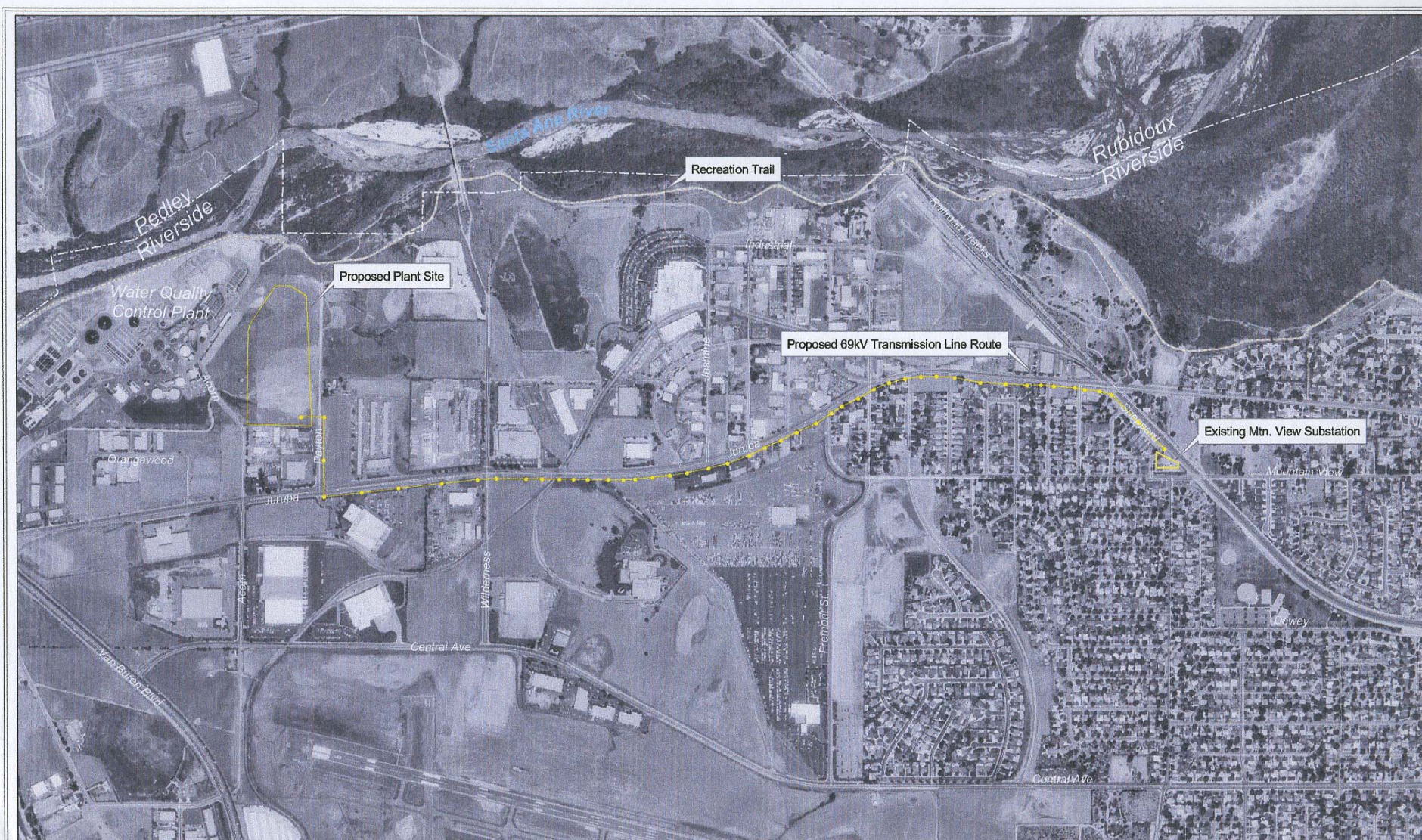
- 59) Please provide an analysis of the impact of Project construction and operation on recreational opportunities in the Hidden Valley Wildlife Area.






**Response:** The Hidden Valley Wildlife Area is located approximately 1 mile due west of the project site. We do not believe there will be any significant impacts to the wildlife area. The attached Map 2 shows the location of the Hidden Valley Wildlife area in relation to the proposed plant site.

# **CURE Data Requests Set 3**

## **Land Use – Map #1**





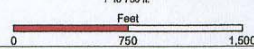
-  Recreation trail
-  Proposed 69kV Transmission line
-  Existing Mtn. View Substation
-  Proposed Site
-  Adjacent to 5950 Acorn

# Riverside Energy Resource Center

Figure 1 - Project Overview



Scale 1:3,000  
1" = 750 ft.



101414 Riverside Energy, Riverside serial.mxd, rev4 7-07-04 jlm



# **CURE Data Requests Set 3**

## **Noise - Attachment 1**

## LT-1 Hourly Long-Term Noise Data

LT-1, rear yard of 6495 Thunder Bay Terrace, north of plant  
Microphone at 1st floor elevation (5' above ground)

Date	Time	Measured 1-Hour Noise Levels, dB(A)			
		Leq	L10	L50	L90
3/15/04	15:00:00	63.5	56.3	44.4	41.5
3/15/04	16:00:00	57.9	54.8	44.7	41.5
3/15/04	17:00:00	59.1	56.4	47.1	43.4
3/15/04	18:00:00	61.5	50.1	43.9	41.1
3/15/04	19:00:00	56.4	51.0	44.1	40.8
3/15/04	20:00:00	61.5	57.5	42.6	40.0
3/15/04	21:00:00	56.7	45.4	40.9	39.0
3/15/04	22:00:00	62.8	58.6	43.0	40.1
3/15/04	23:00:00	60.6	46.7	41.8	39.6
3/16/04	0:00:00	41.6	42.7	40.5	39.0
3/16/04	1:00:00	58.7	48.7	41.2	38.8
3/16/04	2:00:00	59.4	42.6	39.7	37.7
3/16/04	3:00:00	40.9	41.9	40.3	38.6
3/16/04	4:00:00	64.3	53.4	44.0	42.0
3/16/04	5:00:00	61.4	52.4	46.7	43.3
3/16/04	6:00:00	58.7	53.4	47.9	46.0
3/16/04	7:00:00	62.9	53.6	48.0	46.3
3/16/04	8:00:00	58.4	57.7	48.0	45.1
3/16/04	9:00:00	61.9	50.8	44.8	41.5
3/16/04	10:00:00	59.9	51.1	44.3	40.8
3/16/04	11:00:00	55.0	51.9	46.9	42.6
3/16/04	12:00:00	63.4	63.2	47.7	43.4
3/16/04	13:00:00	61.2	52.6	43.4	39.3
3/16/04	14:00:00	50.7	50.7	42.2	38.0
3/16/04	15:00:00	61.2	50.6	40.7	37.5

## LT-1 Hourly Long-Term Noise Data

LT-1, rear yard of 6495 Thunder Bay Terrace, north of plant  
Microphone at 2nd floor elevation (15' above ground)

Date	Time	Measured 1-Hour Noise Levels, dB(A)			
		Leq	L10	L50	L90
3/15/04	15:00:00	71.4	58.4	48.7	46.3
3/15/04	16:00:00	64.6	56.9	48.8	46.3
3/15/04	17:00:00	65.8	59.8	51.5	48.3
3/15/04	18:00:00	69.1	55.9	50.4	46.9
3/15/04	19:00:00	65.4	56.1	50.7	46.8
3/15/04	20:00:00	67.9	66.1	47.9	45.3
3/15/04	21:00:00	64.9	51.2	46.9	44.6
3/15/04	22:00:00	69.9	67.7	50.0	46.2
3/15/04	23:00:00	70.5	53.8	48.0	44.6
3/16/04	0:00:00	46.1	47.8	45.1	43.3
3/16/04	1:00:00	67.3	54.8	45.5	43.1
3/16/04	2:00:00	66.7	47.7	43.9	41.6
3/16/04	3:00:00	45.0	45.8	44.3	42.6
3/16/04	4:00:00	72.0	58.1	47.8	46.1
3/16/04	5:00:00	71.2	54.8	50.4	47.0
3/16/04	6:00:00	67.9	56.6	52.1	50.2
3/16/04	7:00:00	68.6	56.0	52.1	50.3
3/16/04	8:00:00	64.2	61.2	52.0	49.8
3/16/04	9:00:00	68.9	53.4	48.8	45.7
3/16/04	10:00:00	67.1	54.0	48.5	45.3
3/16/04	11:00:00	64.1	54.6	50.4	47.1
3/16/04	12:00:00	71.2	71.2	50.7	47.2
3/16/04	13:00:00	70.1	57.2	47.2	43.6
3/16/04	14:00:00	57.3	52.6	45.9	42.7
3/16/04	15:00:00	70.2	52.8	44.3	41.5

## LT-2 Hourly Long-Term Noise Data

LT-2, rear yard of 8838 Alabama Street, west of plant  
Microphone at 1st floor elevation (5' above ground)

Date	Time	Measured 1-Hour Noise Levels, dB(A)			
		Leq	L10	L50	L90
3/16/04	18:00:00	51.5	53.8	47.2	43.4
3/16/04	19:00:00	55.6	54.7	44.9	42.3
3/16/04	20:00:00	51.7	51.7	45.3	43.3
3/16/04	21:00:00	50.0	50.8	47.3	44.8
3/16/04	22:00:00	53.2	48.5	46.2	44.5
3/16/04	23:00:00	46.2	46.7	44.7	43.3
3/17/04	0:00:00	44.7	46.5	44.3	41.4
3/17/04	1:00:00	45.2	47.0	43.6	41.5
3/17/04	2:00:00	45.8	48.1	43.8	41.4
3/17/04	3:00:00	47.4	49.9	46.3	43.7
3/17/04	4:00:00	50.9	52.9	50.1	47.1
3/17/04	5:00:00	55.2	57.0	53.5	49.5
3/17/04	6:00:00	55.6	56.9	53.9	51.6
3/17/04	7:00:00	58.6	62.7	54.8	50.8
3/17/04	8:00:00	54.4	58.2	50.5	46.2
3/17/04	9:00:00	57.1	61.0	52.7	43.8
3/17/04	10:00:00	55.8	59.6	48.0	40.1
3/17/04	11:00:00	54.3	56.9	44.7	39.4
3/17/04	12:00:00	50.2	50.6	45.1	40.5
3/17/04	13:00:00	48.9	51.0	43.3	38.6
3/17/04	14:00:00	54.9	53.8	42.9	37.1
3/17/04	15:00:00	57.6	57.1	49.9	44.1
3/17/04	16:00:00	48.5	51.7	45.2	42.4
3/17/04	17:00:00	59.4	55.3	47.4	43.6
3/17/04	18:00:00	53.2	53.3	45.2	42.7

## LT-2 Hourly Long-Term Noise Data

LT-2, rear yard of 8838 Alabama Street, west of plant  
Microphone at 2nd floor elevation (15' above ground)

Date	Time	Measured 1-Hour Noise Levels, dB(A)			
		Leq	L10	L50	L90
3/16/04	18:00:00	56.1	58.4	51.5	46.4
3/16/04	19:00:00	56.8	57.5	48.5	45.9
3/16/04	20:00:00	53.8	54.4	49.0	46.3
3/16/04	21:00:00	52.8	54.4	50.8	48.1
3/16/04	22:00:00	58.7	52.3	49.9	48.3
3/16/04	23:00:00	50.2	50.0	48.2	46.8
3/17/04	0:00:00	48.3	49.6	47.4	44.2
3/17/04	1:00:00	48.0	49.9	46.2	43.8
3/17/04	2:00:00	49.2	50.3	46.3	44.2
3/17/04	3:00:00	49.7	52.0	48.8	46.3
3/17/04	4:00:00	53.8	55.6	52.5	49.3
3/17/04	5:00:00	56.6	57.8	55.2	52.0
3/17/04	6:00:00	57.8	59.3	56.3	54.2
3/17/04	7:00:00	59.8	63.2	56.5	53.3
3/17/04	8:00:00	55.4	58.7	52.7	49.4
3/17/04	9:00:00	57.2	60.9	53.1	47.0
3/17/04	10:00:00	55.3	59.4	48.9	43.5
3/17/04	11:00:00	54.3	57.4	47.2	42.7
3/17/04	12:00:00	52.8	52.8	46.1	42.2
3/17/04	13:00:00	50.2	52.1	44.6	40.8
3/17/04	14:00:00	55.6	55.4	45.3	39.8
3/17/04	15:00:00	59.5	59.8	51.1	46.5
3/17/04	16:00:00	51.4	53.9	47.6	44.9
3/17/04	17:00:00	65.5	57.2	49.8	46.2
3/17/04	18:00:00	57.8	57.6	48.8	45.7



### LT-3 Hourly Long-Term Noise Data

LT-3, rear yard of 6401 Vickers Drive, southeast of plant  
Microphone at 1st floor elevation (5' above ground)

Date	Time	Measured 1-Hour Noise Levels, dB(A)			
		Leq	L10	L50	L90
3/18/04	9:00:00	48.0	49.3	44.2	42.4
3/18/04	10:00:00	54.2	50.7	45.2	42.7
3/18/04	11:00:00	50.8	51.0	44.6	42.2
3/18/04	12:00:00	49.3	50.3	45.0	42.2
3/18/04	13:00:00	49.3	51.2	47.0	44.6
3/18/04	14:00:00	49.8	52.6	47.9	45.6
3/18/04	15:00:00	50.0	52.0	48.5	46.2
3/18/04	16:00:00	52.1	52.9	48.2	45.7
3/18/04	17:00:00	49.9	51.9	47.2	45.4
3/18/04	18:00:00	52.7	51.4	46.7	43.8
3/18/04	19:00:00	45.1	46.9	43.8	42.1
3/18/04	20:00:00	45.0	46.8	43.8	42.2
3/18/04	21:00:00	50.4	53.1	46.4	43.8
3/18/04	22:00:00	43.8	45.6	42.9	40.5
3/18/04	23:00:00	39.6	41.5	38.6	35.6
3/19/04	0:00:00	37.6	38.5	34.0	32.3
3/19/04	1:00:00	34.1	34.8	32.2	30.8
3/19/04	2:00:00	31.2	32.8	30.8	28.5
3/19/04	3:00:00	36.3	34.2	31.2	29.8
3/19/04	4:00:00	36.6	38.1	33.8	32.1
3/19/04	5:00:00	39.4	42.1	37.0	34.2
3/19/04	6:00:00	42.0	44.7	40.4	37.2
3/19/04	7:00:00	42.6	44.8	39.7	37.0
3/19/04	8:00:00	45.5	48.3	43.5	40.1
3/19/04	9:00:00	47.7	49.8	45.4	43.6

### LT-3 Hourly Long-Term Noise Data

LT-3, rear yard of 6401 Vickers Drive, southeast of plant  
Microphone at 2nd floor elevation (15' above ground)

Date	Time	Measured 1-Hour Noise Levels, dB(A)			
		Leq	L10	L50	L90
3/18/04	9:00:00	52.1	53.5	49.5	47.7
3/18/04	10:00:00	55.5	53.8	49.4	47.1
3/18/04	11:00:00	52.5	53.9	49.1	45.9
3/18/04	12:00:00	52.5	53.9	48.8	46.4
3/18/04	13:00:00	53.5	56.5	51.4	48.2
3/18/04	14:00:00	53.4	56.1	52.1	49.3
3/18/04	15:00:00	53.5	56.1	52.0	49.3
3/18/04	16:00:00	54.5	56.4	52.0	48.5
3/18/04	17:00:00	52.4	54.9	50.3	48.0
3/18/04	18:00:00	54.6	54.3	49.5	46.4
3/18/04	19:00:00	48.0	50.2	46.6	44.8
3/18/04	20:00:00	47.6	49.4	46.3	44.6
3/18/04	21:00:00	52.7	55.6	49.0	46.2
3/18/04	22:00:00	47.5	48.7	45.3	43.1
3/18/04	23:00:00	44.2	45.4	42.4	41.0
3/19/04	0:00:00	43.4	43.2	36.6	35.1
3/19/04	1:00:00	39.5	39.0	35.6	33.7
3/19/04	2:00:00	35.3	37.7	34.5	31.8
3/19/04	3:00:00	41.9	37.6	34.3	33.0
3/19/04	4:00:00	41.7	42.8	37.2	34.9
3/19/04	5:00:00	43.6	46.5	40.6	37.5
3/19/04	6:00:00	48.2	51.7	45.7	41.2
3/19/04	7:00:00	48.2	51.5	44.5	41.6
3/19/04	8:00:00	50.0	53.1	48.0	44.1
3/19/04	9:00:00	52.0	53.7	49.7	47.4

## Noise Survey Sheet

Project: Riverside Energy Resource Center

Position: LT-1: rear yard of 6495 Thunder Bay Trail,  
12' behind block wall adjacent to RR track

Date: March 15-16, 2004 (25-hour measurement)

Noise Source: Trains, industry, aircraft

SLM Height: 5' and 15'

LD 820 S/N: 0997 at 5', 0996 at 15'

LD CAL200

Calibrator S/N: 2916

Temperature: 72 F

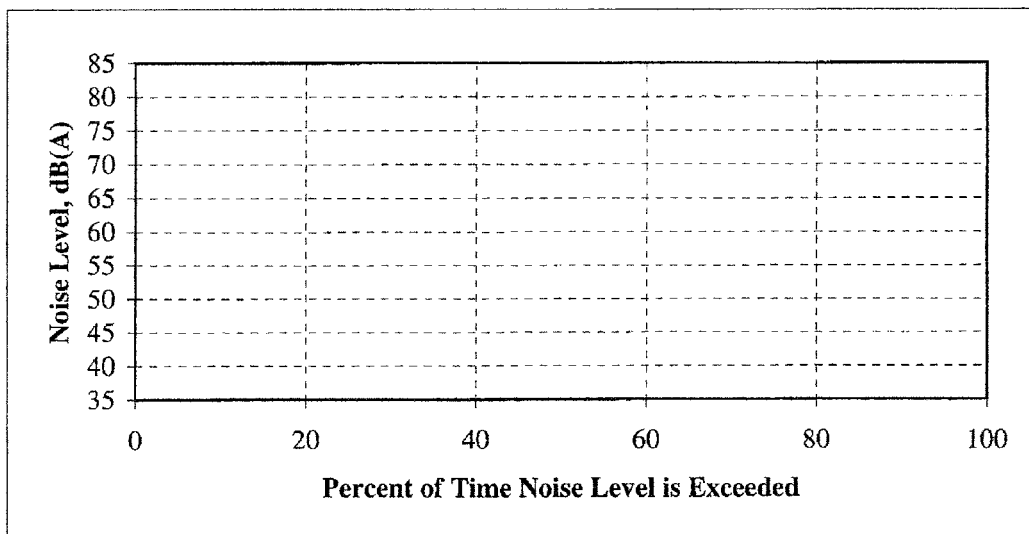
Wind Speed: 3 mph

Wind Direction: West

Humidity: 45%

Operator: Cynthia M. Bordash

	3:00 PM to 3:00 PM
L10	
L50	
L90	
Leq	
Lmax	
Lmin	



## Noise Survey Sheet

Project: Riverside Energy Resource Center

Position: LT-2: rear yard of 8838 Alabama Street,  
11' behind block wall

Date: March 16-17, 2004 (25-hour measurement)

Noise Source: Traffic, aircraft, park activities

SLM Height: 5' and 15'

LD 820 S/N: 0996 at 5', 0997 at 15'

LD CAL200

Calibrator S/N: 2916

Temperature: 91 F

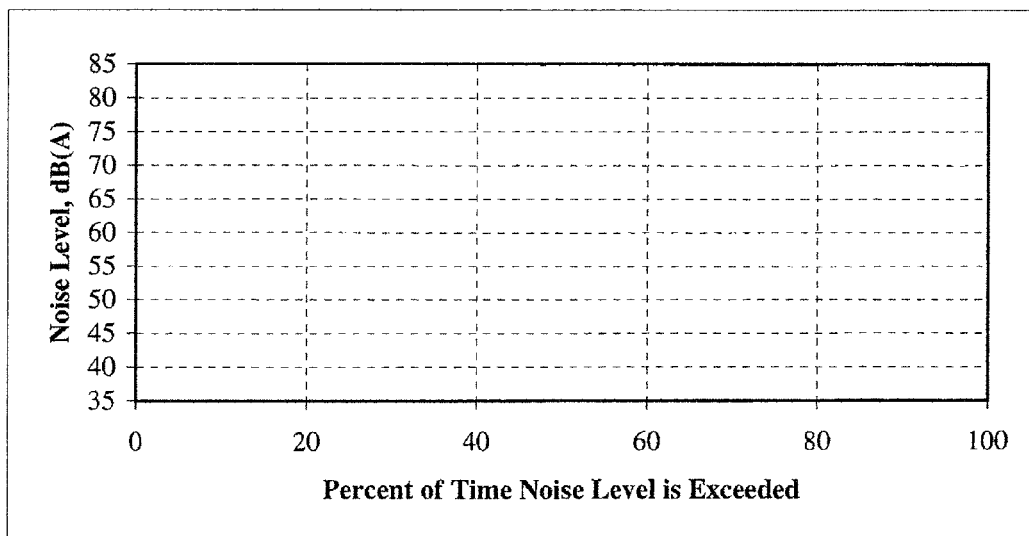
Wind Speed: Calm

Wind Direction: N/A

Humidity: 60%

Operator: Cynthia M. Bordash

	6:00 PM to 6:00 PM
L10	
L50	
L90	
Leq	
Lmax	
Lmin	



## Noise Survey Sheet

Project: Riverside Energy Resource Center

Position: LT-3: rear yard of 6401 Vickers Drive,  
26' behind block wall

Date: March 18-19, 2004 (25-hour measurement)

Noise Source: Traffic, aircraft

SLM Height: 5' and 15'

LD 820 S/N: 0996 at 5', 0997 at 15'

LD CAL200

Calibrator S/N: 2916

Temperature: 48 F

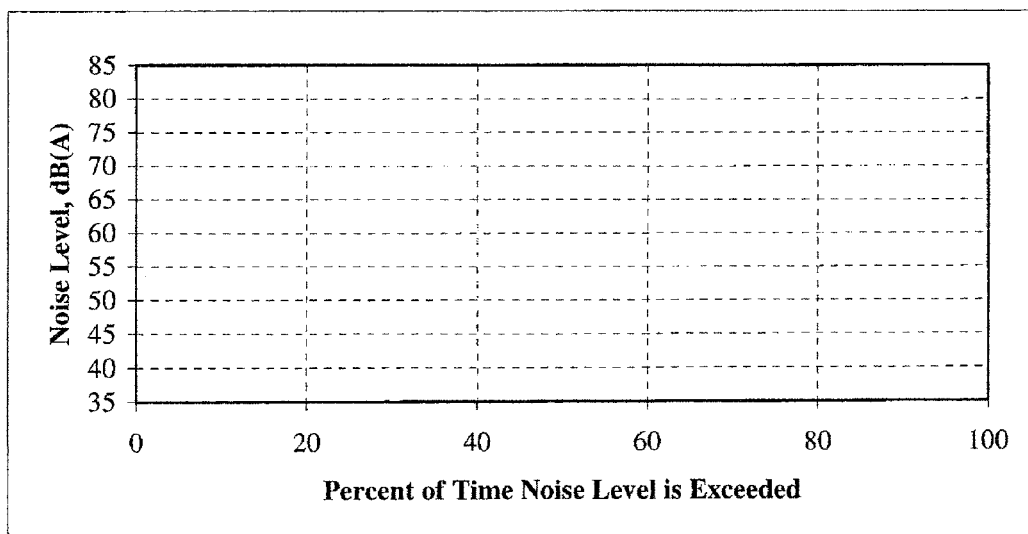
Wind Speed: Calm

Wind Direction: N/A

Humidity: 55%

Operator: Cynthia M. Bordash

	9:00 AM to 9:00 AM
L10	
L50	
L90	
Leq	
Lmax	
Lmin	



# **CURE Data Requests Set 3**

## **Noise - Attachment 2**

## Noise Survey Sheet

Project: Riverside Energy Resource Center

Position: ST-1, Clay Park, 117' from Carlyle Drive,  
200' from Easton

Date: March 16, 2004

Noise Source: Traffic, aircraft, trains, dogs, birds

SLM Height: 5'

LD 712 S/N: 0555

LD CAL200

Calibrator S/N: 2916

Temperature: 54 F

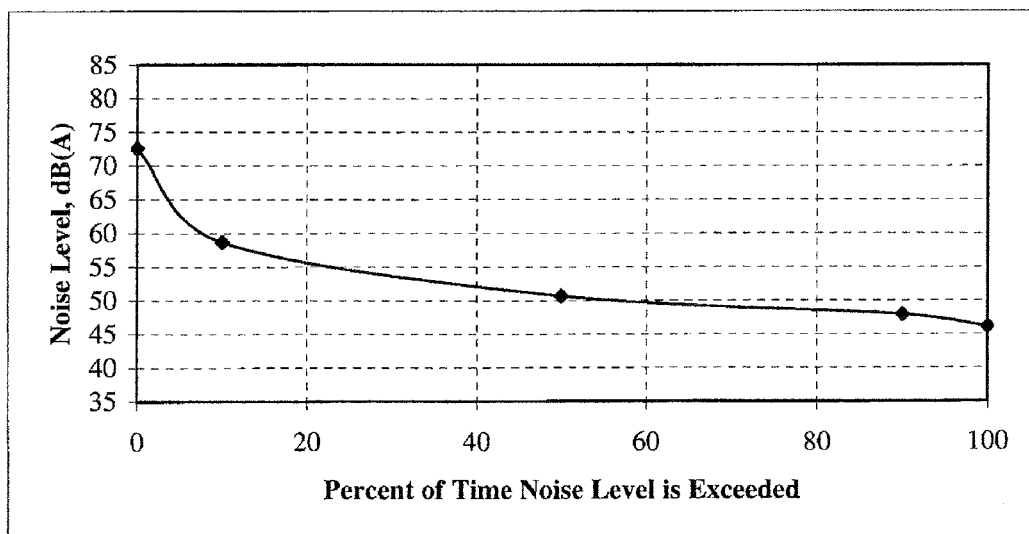
Wind Speed: 6 mph

Wind Direction: West

Humidity: 32%

Operator: Cynthia M. Bordash

	10:22 AM to 10:43 AM
L10	58.7
L50	50.7
L90	47.9
Leq	55.6
Lmax	72.6
Lmin	46.1



## Noise Survey Sheet

Project: Riverside Energy Resource Center

Position: ST-2, Indian Hill School, 4' from High Prairie Tr.,  
208' from Grand Valley

Date: March 17, 2004

Noise Source: Traffic, children

SLM Height: 5'

LD 712 S/N: 0555

LD CAL200

Calibrator S/N: 2916

Temperature: 56 F

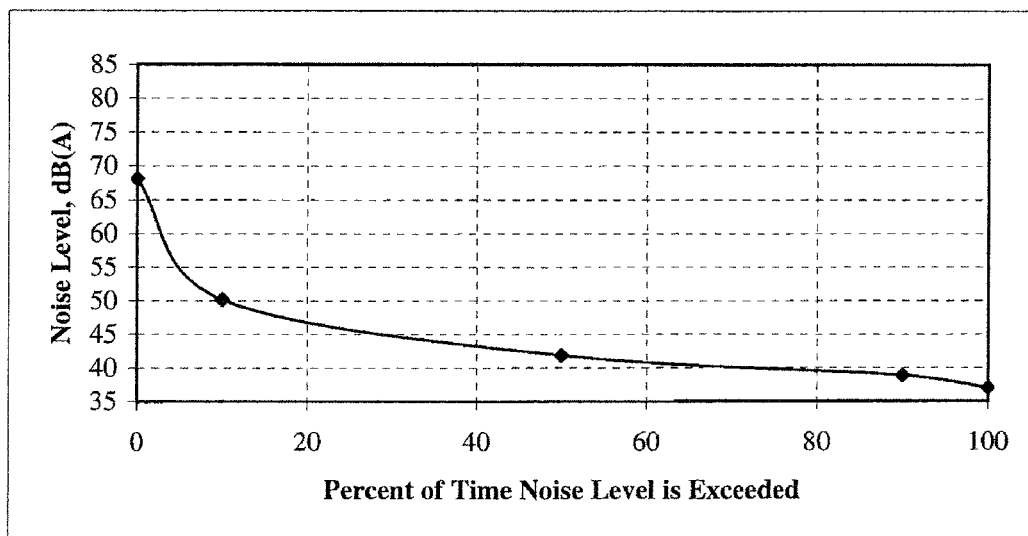
Wind Speed: Calm

Wind Direction: N/A

Humidity: 32%

Operator: Cynthia M. Bordash

	10:15 AM to 10:37 AM
L10	50.2
L50	41.9
L90	38.9
Leq	48.3
Lmax	68.1
Lmin	37.0





## Noise Survey Sheet

Project: Riverside Energy Resource Center

Position: ST-3, front yard at 7982 Claudette, 7' from curb

Date: March 16, 2004

Noise Source: Traffic, aircraft, trains, industry, birds

SLM Height: 5'

LD 712 S/N: 0555

LD CAL200

Calibrator S/N: 2916

Temperature: 51 F

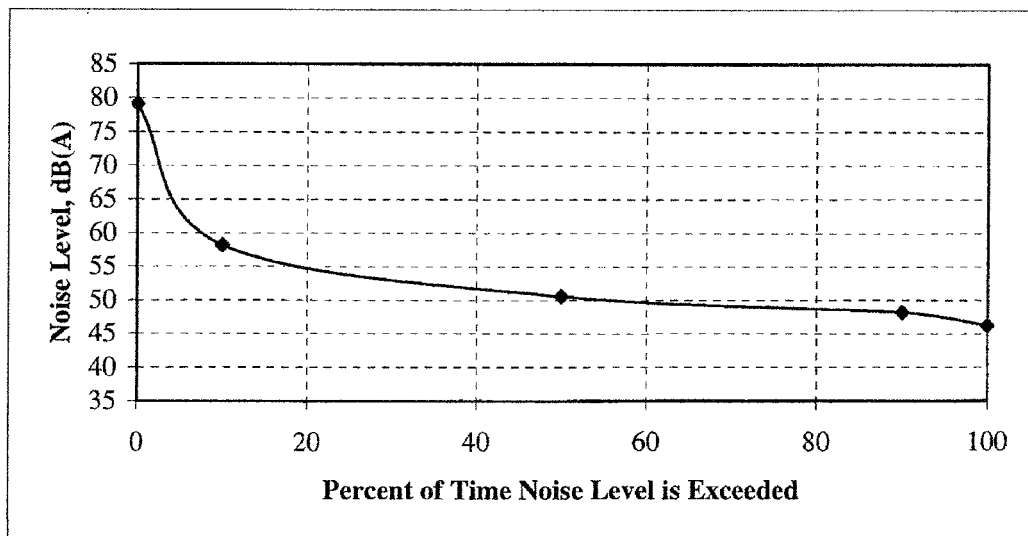
Wind Speed: 9 mph

Wind Direction: West

Humidity: 42%

Operator: Cynthia M. Bordash

	9:01 AM to 9:22 AM
L10	58.2
L50	50.6
L90	48.2
Leq	60.8
Lmax	79.1
Lmin	46.2



## Noise Survey Sheet

Project: Riverside Energy Resource Center

Position: ST-4, at 6465 Avenue Juan Diaz, 70 yards from the house

Date: March 17, 2004

Noise Source: Traffic, aircraft, trains, birds, dogs

SLM Height: 5'

LD 712 S/N: 0555

LD CAL200

Calibrator S/N: 2916

Temperature: 90 F

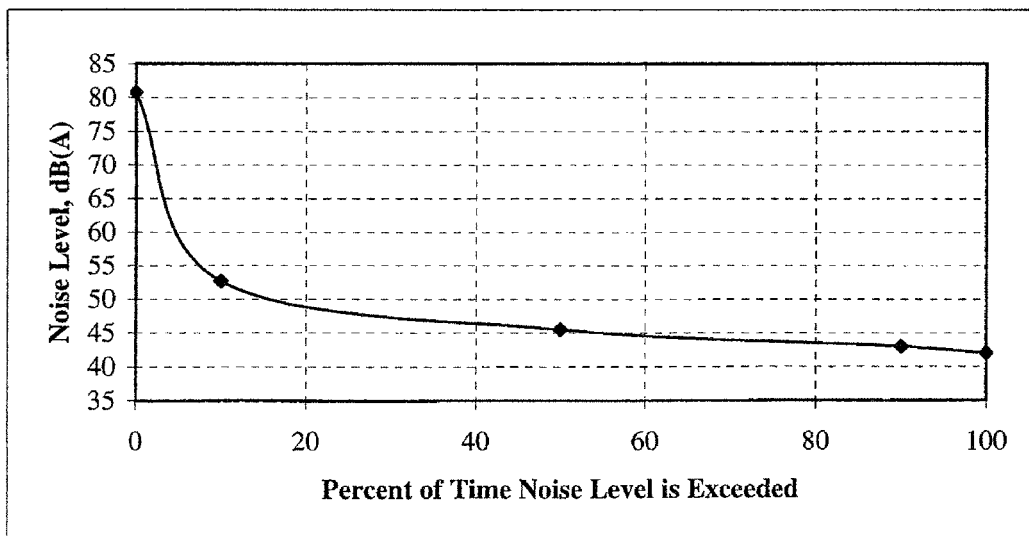
Wind Speed: Calm

Wind Direction: N/A

Humidity: 60%

Operator: Cynthia M. Bordash

	6:06 PM to 6:26 PM
L10	52.7
L50	45.5
L90	43.0
Leq	56.8
Lmax	80.8
Lmin	42.0



## Noise Survey Sheet

Project: Riverside Energy Resource Center

Position: ST-5, on recreational trail north of project site

Date: March 17, 2004

Noise Source: Traffic, aircraft, trains, birds, industry

SLM Height: 5'

LD 712 S/N: 0555

LD CAL200

Calibrator S/N: 2916

Temperature: 87 F

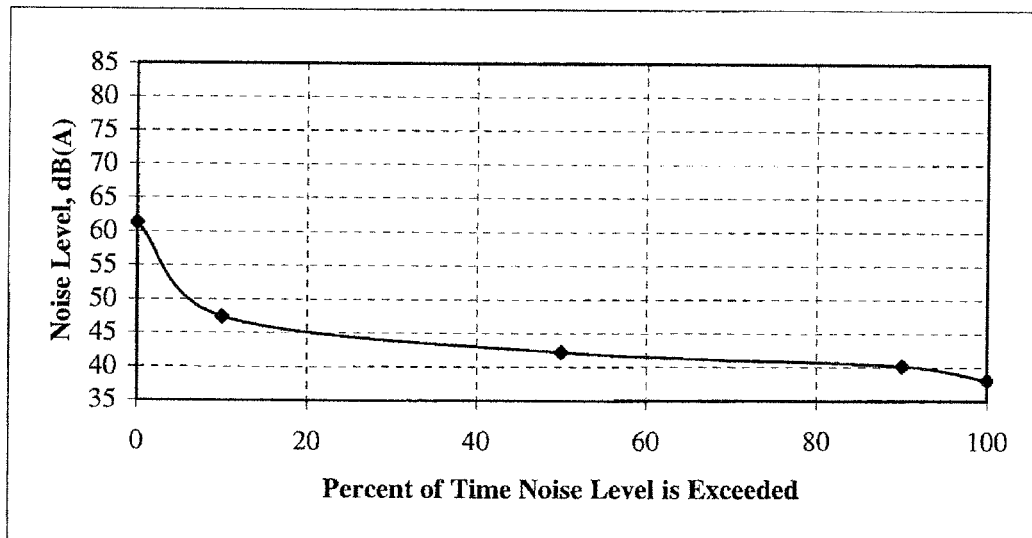
Wind Speed: Calm

Wind Direction: N/A

Humidity: 27%

Operator: Cynthia M. Bordash

	2:12 PM to 2:32 PM
L10	47.4
L50	42.2
L90	40.2
Leq	45.5
Lmax	61.3
Lmin	38.1



## Noise Survey Sheet

Project: Riverside Energy Resource Center

Position: ST-6, at administrative offices of wastewater treatment plant

Date: March 16, 2004

Noise Source: Industry, train, cars in parking lot

SLM Height: 5'

LD 712 S/N: 0555

LD CAL200

Calibrator S/N: 2916

Temperature: 74 F

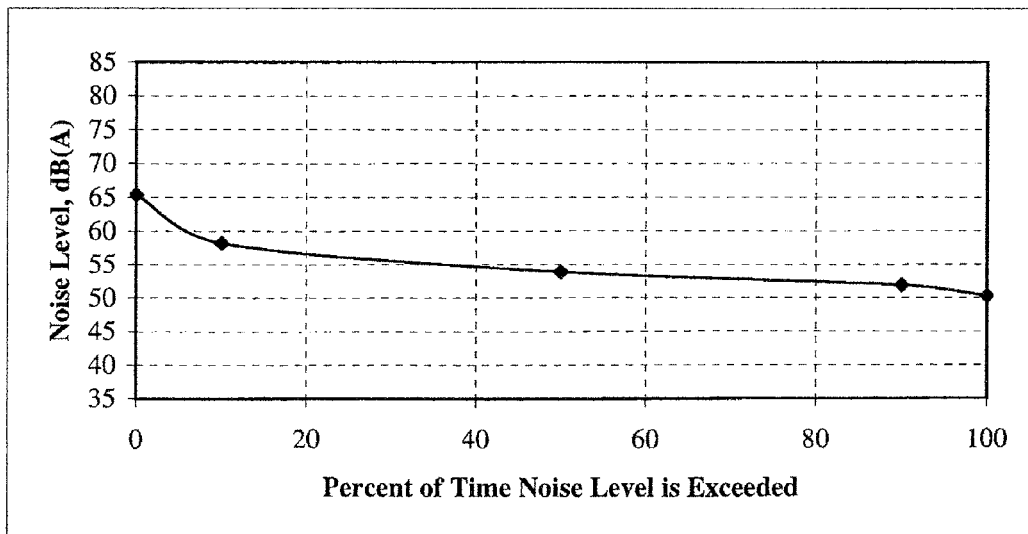
Wind Speed: 6 mph

Wind Direction: East

Humidity: 26%

Operator: Cynthia M. Bordash

	12:17 PM to 12:37 PM
L10	58.2
L50	53.9
L90	51.9
Leq	55.4
Lmax	65.4
Lmin	50.3



## Noise Survey Sheet

Project: Riverside Energy Resource Center

Position: ST-7, at the Maaco facility, 5925 Payton Ave.,  
30' from property line fence

Date: March 16, 2004

Noise Source: Industry, train, cars in parking lot

SLM Height: 5'

LD 712 S/N: 0555

LD CAL200  
Calibrator S/N: 2916

Temperature: 86 F

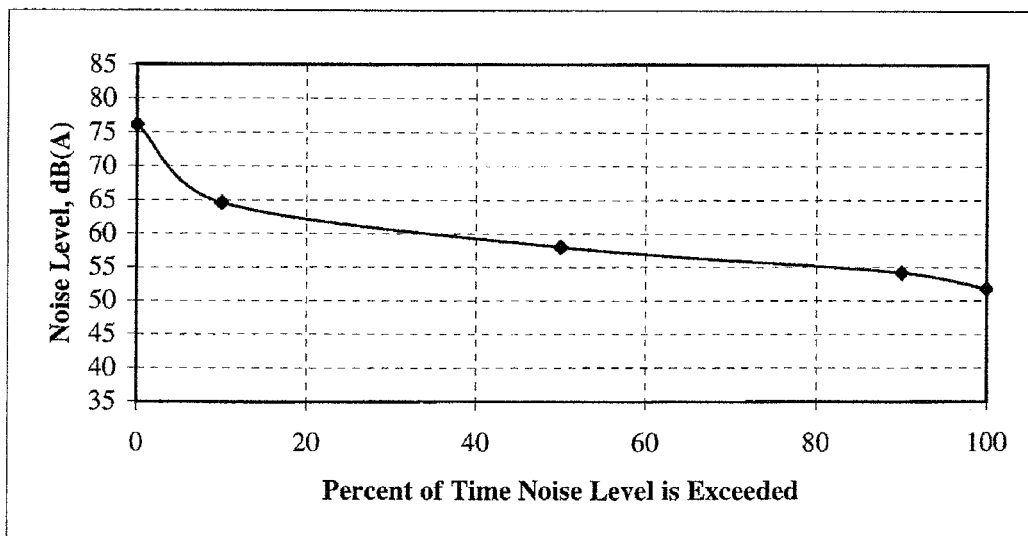
Wind Speed: 9 mph

Wind Direction: South

Humidity: 26%

Operator: Cynthia M. Bordash

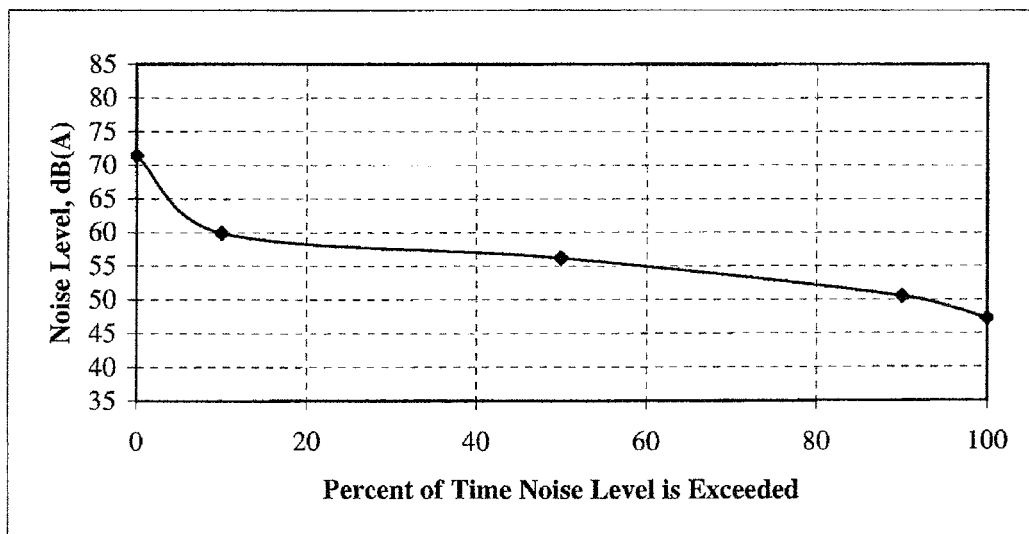
	1:04 PM to 1:24 PM
L10	64.6
L50	58.0
L90	54.2
Leq	61.1
Lmax	76.1
Lmin	51.8



## Noise Survey Sheet

Project: Riverside Energy Resource Center  
 Position: ST-8, industrial facility at 7171 Jurupa Ave.,  
 Unit 30  
 Date: March 16, 2004  
 Noise Source: Industry, aircraft, dogs, traffic  
 SLM Height: 5'  
 LD 712 S/N: 0555  
 LD CAL200  
 Calibrator S/N: 2916  
 Temperature: 86 F  
 Wind Speed: 8 mph  
 Wind Direction: South  
 Humidity: 28%  
 Operator: Cynthia M. Bordash

	1:38 PM to 1:59 PM
L10	59.9
L50	56.2
L90	50.5
Leq	57.8
Lmax	71.4
Lmin	47.2



## Noise Survey Sheet

Project: Riverside Energy Resource Center

Position: ST-9, at church building in industrial park, 7110  
Jurupa Ave., Unit 5

Date: March 16, 2004

Noise Source: Industry, aircraft, traffic

SLM Height: 5'

LD 712 S/N: 0555

LD CAL200

Calibrator S/N: 2916

Temperature: 87 F

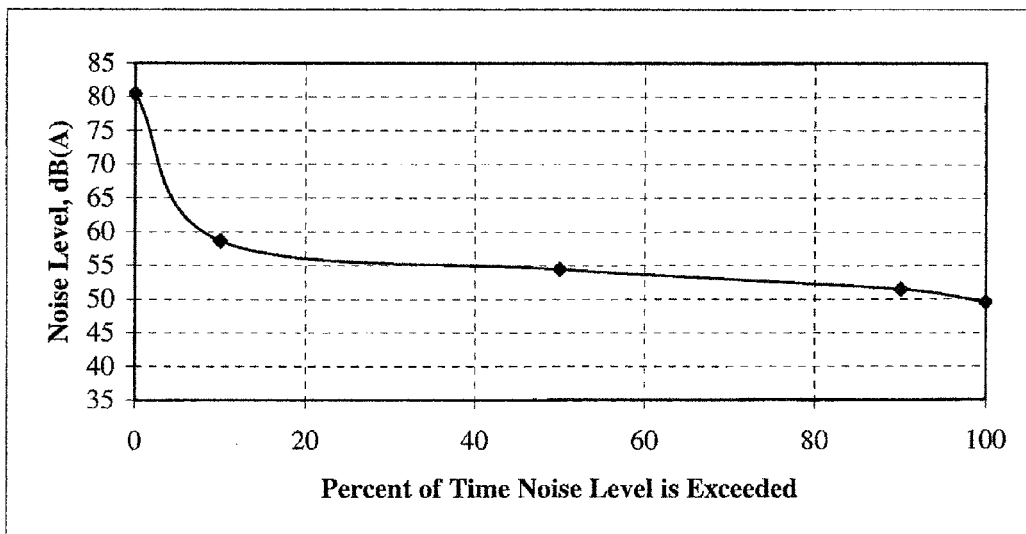
Wind Speed: 6 mph

Wind Direction: West

Humidity: 25%

Operator: Cynthia M. Bordash

	2:19 PM to 2:39 PM
L10	58.7
L50	54.5
L90	51.5
Leq	59.0
Lmax	80.5
Lmin	49.5



## Noise Survey Sheet

Project: Riverside Energy Resource Center

Position: ST-10, residence at 6344 Jurupa Ave.,  
33' from street

Date: March 17, 2004

Noise Source: Traffic

SLM Height: 5'

LD 712 S/N: 0555

LD CAL200

Calibrator S/N: 2916

Temperature: 91 F

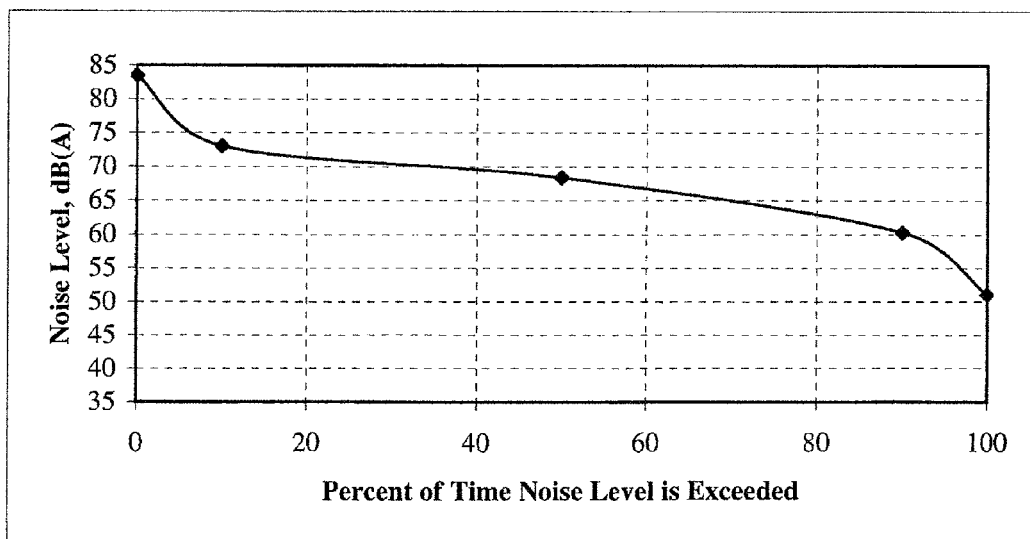
Wind Speed: Calm

Wind Direction: N/A

Humidity: 44%

Operator: Cynthia M. Bordash

	5:02 PM to 5:22 PM
L10	73.0
L50	68.4
L90	60.3
Leq	69.9
Lmax	83.5
Lmin	51.0





## Noise Survey Sheet

Project: Riverside Energy Resource Center

Position: ST-11, residence at 6896 Palos Dr.,  
104' from street

Date: March 17, 2004

Noise Source: Traffic, aircraft

SLM Height: 5'

LD 712 S/N: 0555

LD CAL200  
Calibrator S/N: 2916

Temperature: 65 F

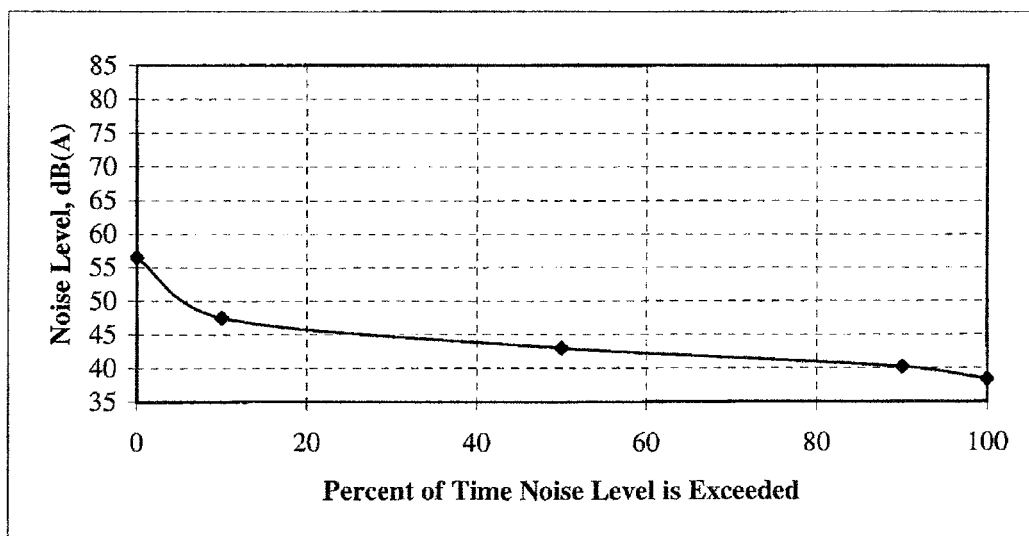
Wind Speed: Calm

Wind Direction: N/A

Humidity: 29%

Operator: Cynthia M. Bordash

	11:14 AM to 11:34 AM
L10	47.5
L50	43.0
L90	40.2
Leq	44.9
Lmax	56.5
Lmin	38.3



## Noise Survey Sheet

Project: Riverside Energy Resource Center

Position: ST-12, residence at 6711 Doolittle Ave.,  
52 yards from street

Date: March 17, 2004

Noise Source: Traffic, aircraft

SLM Height: 5'

LD 712 S/N: 0555

LD CAL200

Calibrator S/N: 2916

Temperature: 88 F

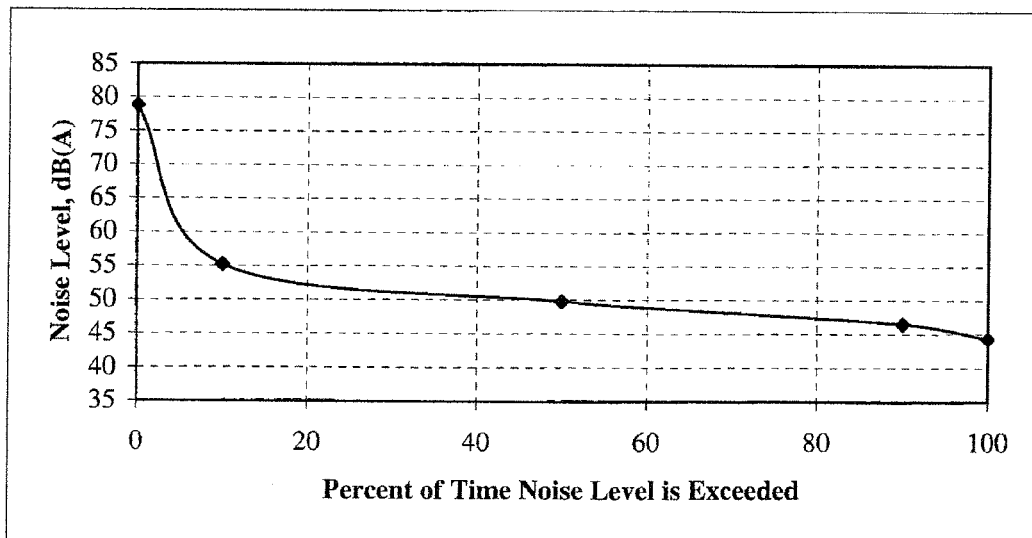
Wind Speed: Calm

Wind Direction: N/A

Humidity: 26%

Operator: Cynthia M. Bordash

	3:01 PM to 3:17 PM
L10	55.2
L50	49.8
L90	46.5
Leq	58.5
Lmax	78.8
Lmin	44.3



# **CURE Data Requests Set 3**

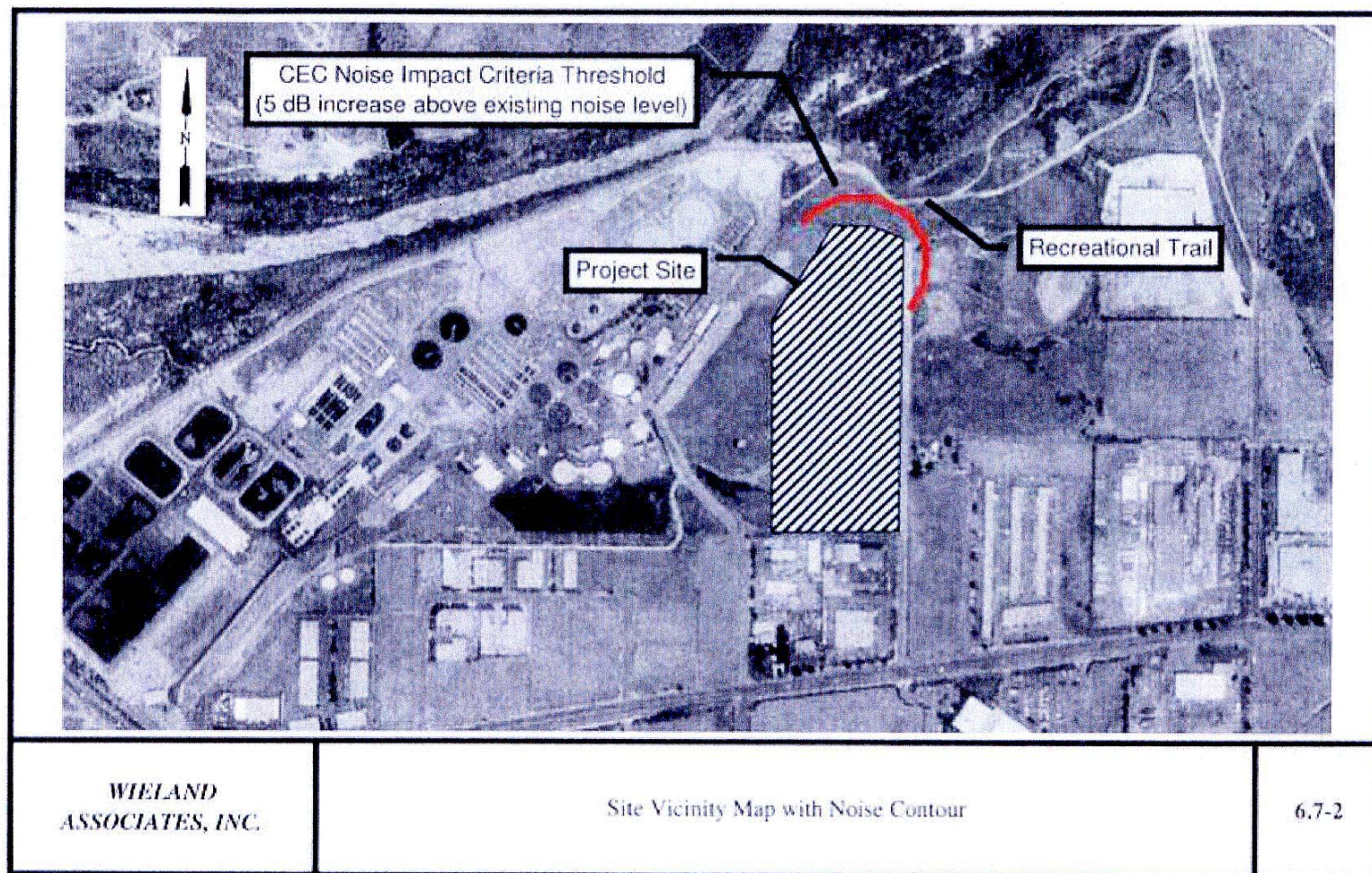
## **Noise - Attachment 3**

**Table 6.7-2 Short-Term Noise Measurements, March 16-17, 2004**

Site ID	Measurement Location	Measurement Period				Measurement Results, dB(A)					
		Date	Start Time	Duration (min)	Predominant Noise Sources	Leq	Lmax	Lmin	L90	L50	L10
ST-1	Clay Park	3/16/04	10:22	21	Traffic, aircraft, trains, birds, dogs	56	73	76	48	51	59
ST-2	Indian Hill School	3/17/04	10:15	22	Traffic, children	48	68	37	39	42	50
ST-3	Residence at 7982 Claudette Dr.	3/16/04	9:01	21	Industrial, traffic, train, aircraft, birds	61	79	46	48	51	59
ST-4	Residence at 6465 Avenue Juan Diaz	3/17/04	18:06	20	Traffic, aircraft, dogs, trains, birds	57	81	42	43	46	53
ST-5	Recreational trail	3/17/04	14:12	20	Industrial, aircraft, trains, birds	46	61	38	40	42	47
ST-6	Administrative offices at water treatment plant	3/16/04	12:17	20	Industrial, trains	55	65	50	52	54	58
ST-7	Maaco, 5925 Payton	3/16/04	13:04	20	Industrial, train, aircraft	61	76	52	54	58	65
ST-8	Industry, 7171 Jurupa, Unit 30	3/16/04	13:38	21	Industrial, aircraft, dogs	58	71	47	51	56	60
ST-9	Church, 7110 Jurupa, Unit 5	3/16/04	14:19	20	Industrial, aircraft, radio	59	81	50	52	55	59
ST-10	Residence, 6344 Jurupa	3/17/04	17:02	20	Traffic	70	84	51	60	68	73
ST-11	Residence, 6896 Palos	3/17/04	11:14	20	Traffic, aircraft	45	57	38	40	43	48
ST-12	Residence, 6711 Doolittle	3/17/04	15:01	16	Traffic, aircraft	59	79	44	47	50	55

# **CURE Data Requests Set 3**

## **Noise - Attachment 4**



# **CURE Data Requests Set 3**

## **Noise - Attachment 5**

Nearest Residential Property: 2,870 Feet North of Nominal Acoustic Center

[illegible]



Standard Lw			111	111	112	110	104	96	92	90	89
Distance Correction			67	67	67	67	67	67	67	67	67
Atmospheric Absorption (59 deg F, 70% RH)			1	1	2	3	5	9	15	30	51
Directivity			0	0	0	0	0	0	0	0	0
<b>Auxiliary Cooling Tower, SPL</b>		<b>34</b>	<b>43</b>	<b>43</b>	<b>43</b>	<b>40</b>	<b>32</b>	<b>21</b>	<b>10</b>	<b>-7</b>	<b>-28</b>
Fuel Gas Compressor Skid	2,870										
Standard Lw			116	116	110	110	108	107	109	108	107
Distance Correction			67	67	67	67	67	67	67	67	67
Atmospheric Absorption (59 deg F, 70% RH)			1	1	2	3	5	9	15	30	51
Directivity			0	0	0	0	0	0	0	0	0
<b>Fuel Gas Compressor Skid, SPL</b>		<b>38</b>	<b>48</b>	<b>47</b>	<b>41</b>	<b>40</b>	<b>36</b>	<b>31</b>	<b>27</b>	<b>11</b>	<b>-11</b>
Tempering Air Fans	2,870										
Standard Lw			109	107	105	101	97	96	88	84	84
Distance Correction			67	67	67	67	67	67	67	67	67
Atmospheric Absorption (59 deg F, 70% RH)			1	1	2	3	5	9	15	30	51
Directivity			0	0	0	0	0	0	0	0	0
<b>Tempering Air Fans, SPL</b>		<b>27</b>	<b>41</b>	<b>39</b>	<b>36</b>	<b>31</b>	<b>25</b>	<b>21</b>	<b>6</b>	<b>-13</b>	<b>-33</b>

**Nearest Residential Property: 4,130 Feet Southwest of Nominal Acoustic Center**

[illegible]

Standard Lw			111	111	112	110	104	96	92	90	89
Distance Correction			70	70	70	70	70	70	70	70	70
Atmospheric Absorption (59 deg F, 70% RH)			1	2	3	5	7	12	21	44	73
Directivity			0	0	0	0	0	0	0	0	0
<b>Auxiliary Cooling Tower, SPL</b>		<b>30</b>	<b>40</b>	<b>39</b>	<b>39</b>	<b>35</b>	<b>27</b>	<b>14</b>	<b>1</b>	<b>-24</b>	<b>-54</b>
Fuel Gas Compressor Skid	4,130										
Standard Lw			116	116	110	110	108	107	109	108	107
Distance Correction			70	70	70	70	70	70	70	70	70
Atmospheric Absorption (59 deg F, 70% RH)			1	2	3	5	7	12	21	44	73
Directivity			0	0	0	0	0	0	0	0	0
<b>Fuel Gas Compressor Skid, SPL</b>		<b>32</b>	<b>45</b>	<b>44</b>	<b>37</b>	<b>35</b>	<b>31</b>	<b>25</b>	<b>18</b>	<b>-5</b>	<b>-36</b>
Tempering Air Fans	4,130										
Standard Lw			109	107	105	101	97	96	88	84	84
Distance Correction			70	70	70	70	70	70	70	70	70
Atmospheric Absorption (59 deg F, 70% RH)			1	2	3	5	7	12	21	44	73
Directivity			0	0	0	0	0	0	0	0	0
<b>Tempering Air Fans, SPL</b>		<b>22</b>	<b>38</b>	<b>35</b>	<b>32</b>	<b>26</b>	<b>20</b>	<b>14</b>	<b>-3</b>	<b>-30</b>	<b>-59</b>

Nearest Residential Property: 4,200 Feet Southeast of Nominal Acoustic Center

[illegible]

Standard Lw			111	111	112	110	104	96	92	90	89
Distance Correction			70	70	70	70	70	70	70	70	70
Atmospheric Absorption (59 deg F, 70% RH)			1	2	3	5	8	13	22	44	74
Directivity			0	0	0	0	0	0	0	0	0
<b>Auxiliary Cooling Tower, SPL</b>		<b>29</b>	<b>40</b>	<b>39</b>	<b>38</b>	<b>35</b>	<b>26</b>	<b>13</b>	<b>0</b>	<b>-24</b>	<b>-55</b>
Fuel Gas Compressor Skid	4,200										
Standard Lw			116	116	110	110	108	107	109	108	107
Distance Correction			70	70	70	70	70	70	70	70	70
Atmospheric Absorption (59 deg F, 70% RH)			1	2	3	5	8	13	22	44	74
Directivity			0	0	0	0	0	0	0	0	0
<b>Fuel Gas Compressor Skid, SPL</b>		<b>32</b>	<b>45</b>	<b>43</b>	<b>37</b>	<b>35</b>	<b>31</b>	<b>24</b>	<b>17</b>	<b>-6</b>	<b>-38</b>
Tempering Air Fans	4,200										
Standard Lw			109	107	105	101	97	96	88	84	84
Distance Correction			70	70	70	70	70	70	70	70	70
Atmospheric Absorption (59 deg F, 70% RH)			1	2	3	5	8	13	22	44	74
Directivity			0	0	0	0	0	0	0	0	0
<b>Tempering Air Fans, SPL</b>		<b>22</b>	<b>38</b>	<b>35</b>	<b>31</b>	<b>26</b>	<b>19</b>	<b>13</b>	<b>-4</b>	<b>-30</b>	<b>-60</b>

Nearest Residential Property: 4,000 Feet South of Nominal Acoustic Center

[illegible]

Standard Lw			111	111	112	110	104	96	92	90	89
Distance Correction			70	70	70	70	70	70	70	70	70
Atmospheric Absorption (59 deg F, 70% RH)			1	2	3	5	7	12	21	42	71
Directivity			0	0	0	0	0	0	0	0	0
<b>Auxiliary Cooling Tower, SPL</b>		<b>30</b>	<b>40</b>	<b>39</b>	<b>39</b>	<b>36</b>	<b>27</b>	<b>14</b>	<b>2</b>	<b>-22</b>	<b>-51</b>
Fuel Gas Compressor Skid	4,000										
Standard Lw			116	116	110	110	108	107	109	108	107
Distance Correction			70	70	70	70	70	70	70	70	70
Atmospheric Absorption (59 deg F, 70% RH)			1	2	3	5	7	12	21	42	71
Directivity			0	0	0	0	0	0	0	0	0
<b>Fuel Gas Compressor Skid, SPL</b>		<b>33</b>	<b>45</b>	<b>44</b>	<b>37</b>	<b>36</b>	<b>32</b>	<b>25</b>	<b>19</b>	<b>-4</b>	<b>-34</b>
Tempering Air Fans	4,000										
Standard Lw			109	107	105	101	97	96	88	84	84
Distance Correction			70	70	70	70	70	70	70	70	70
Atmospheric Absorption (59 deg F, 70% RH)			1	2	3	5	7	12	21	42	71
Directivity			0	0	0	0	0	0	0	0	0
<b>Tempering Air Fans, SPL</b>		<b>23</b>	<b>38</b>	<b>35</b>	<b>32</b>	<b>27</b>	<b>20</b>	<b>14</b>	<b>-2</b>	<b>-28</b>	<b>-56</b>

### Sound Level Calculation

[illegible]



Standard Lw			111	111	112	110	104	96	92	90	89
Distance Correction			72	72	72	72	72	72	72	72	72
Atmospheric Absorption (59 deg F, 70% RH)			2	3	5	7	10	17	29	59	98
Directivity			0	0	0	0	0	0	0	0	0
<b>Auxiliary Cooling Tower, SPL</b>		<b>25</b>	<b>37</b>	<b>36</b>	<b>35</b>	<b>31</b>	<b>22</b>	<b>7</b>	<b>-9</b>	<b>-41</b>	<b>-82</b>
Fuel Gas Compressor Skid	5,550										
Standard Lw			116	116	110	110	108	107	109	108	107
Distance Correction			72	72	72	72	72	72	72	72	72
Atmospheric Absorption (59 deg F, 70% RH)			2	3	5	7	10	17	29	59	98
Directivity			0	0	0	0	0	0	0	0	0
<b>Fuel Gas Compressor Skid, SPL</b>		<b>27</b>	<b>42</b>	<b>40</b>	<b>33</b>	<b>31</b>	<b>26</b>	<b>18</b>	<b>8</b>	<b>-23</b>	<b>-64</b>
Tempering Air Fans	5,550										
Standard Lw			109	107	105	101	97	96	88	84	84
Distance Correction			72	72	72	72	72	72	72	72	72
Atmospheric Absorption (59 deg F, 70% RH)			2	3	5	7	10	17	29	59	98
Directivity			0	0	0	0	0	0	0	0	0
<b>Tempering Air Fans, SPL</b>		<b>18</b>	<b>35</b>	<b>32</b>	<b>28</b>	<b>22</b>	<b>15</b>	<b>7</b>	<b>-13</b>	<b>-47</b>	<b>-87</b>

Nearest Park Property: 3,320 Feet North of Nominal Acoustic Center

[illegible]

Standard Lw			111	111	112	110	104	96	92	90	89
Distance Correction			68	68	68	68	68	68	68	68	68
Atmospheric Absorption (59 deg F, 70% RH)			1	2	3	4	6	10	17	35	59
Directivity			0	0	0	0	0	0	0	0	0
<b>Auxiliary Cooling Tower, SPL</b>		<b>33</b>	<b>42</b>	<b>41</b>	<b>41</b>	<b>38</b>	<b>30</b>	<b>18</b>	<b>7</b>	<b>-13</b>	<b>-38</b>
Fuel Gas Compressor Skid	3,320										
Standard Lw			116	116	110	110	108	107	109	108	107
Distance Correction			68	68	68	68	68	68	68	68	68
Atmospheric Absorption (59 deg F, 70% RH)			1	2	3	4	6	10	17	35	59
Directivity			0	0	0	0	0	0	0	0	0
<b>Fuel Gas Compressor Skid, SPL</b>		<b>36</b>	<b>47</b>	<b>46</b>	<b>39</b>	<b>38</b>	<b>34</b>	<b>29</b>	<b>24</b>	<b>5</b>	<b>-20</b>
Tempering Air Fans	3,320										
Standard Lw			109	107	105	101	97	96	88	84	84
Distance Correction			68	68	68	68	68	68	68	68	68
Atmospheric Absorption (59 deg F, 70% RH)			1	2	3	4	6	10	17	35	59
Directivity			0	0	0	0	0	0	0	0	0
<b>Tempering Air Fans, SPL</b>		<b>25</b>	<b>40</b>	<b>37</b>	<b>34</b>	<b>29</b>	<b>23</b>	<b>18</b>	<b>3</b>	<b>-19</b>	<b>-43</b>

### Sound Level Calculation

[illegible]

Standard Lw			111	111	112	110	104	96	92	90	89
Distance Correction			69	69	69	69	69	69	69	69	69
Atmospheric Absorption (59 deg F, 70% RH)			1	2	3	4	6	11	19	38	64
Directivity			0	0	0	0	0	0	0	0	0
<b>Auxiliary Cooling Tower, SPL</b>		<b>31</b>	<b>41</b>	<b>41</b>	<b>40</b>	<b>37</b>	<b>29</b>	<b>17</b>	<b>5</b>	<b>-17</b>	<b>-43</b>
Fuel Gas Compressor Skid	3,600										
Standard Lw			116	116	110	110	108	107	109	108	107
Distance Correction			69	69	69	69	69	69	69	69	69
Atmospheric Absorption (59 deg F, 70% RH)			1	2	3	4	6	11	19	38	64
Directivity			0	0	0	0	0	0	0	0	0
<b>Fuel Gas Compressor Skid, SPL</b>		<b>34</b>	<b>46</b>	<b>45</b>	<b>38</b>	<b>37</b>	<b>33</b>	<b>27</b>	<b>22</b>	<b>1</b>	<b>-26</b>
Tempering Air Fans	3,600										
Standard Lw			109	107	105	101	97	96	88	84	84
Distance Correction			69	69	69	69	69	69	69	69	69
Atmospheric Absorption (59 deg F, 70% RH)			1	2	3	4	6	11	19	38	64
Directivity			0	0	0	0	0	0	0	0	0
<b>Tempering Air Fans, SPL</b>		<b>24</b>	<b>39</b>	<b>37</b>	<b>33</b>	<b>28</b>	<b>22</b>	<b>17</b>	<b>1</b>	<b>-23</b>	<b>-48</b>

[illegible]

Standard Lw			111	111	112	110	104	96	92	90	89
Distance Correction			59	59	59	59	59	59	59	59	59
Atmospheric Absorption (59 deg F, 70% RH)			0	1	1	1	2	4	6	13	22
Directivity			0	0	0	0	0	0	0	0	0
<b>Auxiliary Cooling Tower, SPL</b>		<b>44</b>	<b>51</b>	<b>51</b>	<b>52</b>	<b>49</b>	<b>42</b>	<b>33</b>	<b>26</b>	<b>18</b>	<b>8</b>
Fuel Gas Compressor Skid	1,220										
Standard Lw			116	116	110	110	108	107	109	108	107
Distance Correction			59	59	59	59	59	59	59	59	59
Atmospheric Absorption (59 deg F, 70% RH)			0	1	1	1	2	4	6	13	22
Directivity			0	0	0	0	0	0	0	0	0
<b>Fuel Gas Compressor Skid, SPL</b>		<b>50</b>	<b>56</b>	<b>56</b>	<b>50</b>	<b>49</b>	<b>47</b>	<b>44</b>	<b>43</b>	<b>36</b>	<b>26</b>
Tempering Air Fans	1,220										
Standard Lw			109	107	105	101	97	96	88	84	84
Distance Correction			59	59	59	59	59	59	59	59	59
Atmospheric Absorption (59 deg F, 70% RH)			0	1	1	1	2	4	6	13	22
Directivity			0	0	0	0	0	0	0	0	0
<b>Tempering Air Fans, SPL</b>		<b>38</b>	<b>49</b>	<b>47</b>	<b>45</b>	<b>40</b>	<b>35</b>	<b>33</b>	<b>22</b>	<b>12</b>	<b>3</b>

Riverside Energy Resource Center  
Sound Level Calculation  
Nearest Recreational Property: 790 Feet North of Nominal Acoustic Center

	Distance (feet)	dBA	OCTAVE BAND CENTER FREQUENCY (Hz)								
			31.5	63	125	250	500	1000	2000	1220	8000
Receptor Location	Varies		67.0	63.3	55.5	50.5	44.6	38.8	39.7	37.1	33.2
		48.5	27.6	37.1	39.4	41.9	41.4	38.8	40.9	38.1	32.1
Summary											
CTG #1 Enclosure	990	32.9	55.1	44.9	45.6	36.2	27.6	18.4	9.2	3.8	-10.3
CTG #1 Inlet Air Filter House	990	25.6	35.2	43.0	35.7	31.3	17.7	8.5	2.4	2.0	-5.0
SCR #1 Main Duct	990	27.4	54.2	47.0	36.7	32.3	19.7	5.5	-4.6	-10.0	-15.0
SCR #1 Stack	990	33.3	60.2	57.0	43.7	31.3	18.7	10.5	3.4	-5.0	-13.0
CTG #2 Enclosure	850	34.5	56.6	46.4	47.1	37.8	29.3	20.3	11.4	6.8	-6.2
CTG #2 Inlet Air Filter House	850	27.1	36.6	44.4	37.1	32.8	19.3	10.3	4.4	4.8	-1.2
SCR #2 Main Duct	850	28.7	55.4	48.3	38.0	33.7	21.2	7.1	-2.7	-7.4	-11.5
SCR #2 Stack	850	34.7	61.4	58.3	45.0	33.7	20.2	13.1	6.3	-0.4	-7.5
Ammonia Evaporation Skid #1	970	28.4	40.4	39.2	36.9	33.5	25.9	16.8	5.6	-3.6	-15.5
Ammonia Evaporation Skid #2	850	29.3	41.6	40.4	38.1	33.8	27.3	18.3	7.4	-1.2	-12.2
Chiller Package	820	27.2	26.9	26.7	23.4	27.1	24.6	21.7	19.9	14.5	-5.4
Auxiliary Cooling Tower	820	39.6	49.9	48.7	48.4	45.1	36.6	25.7	16.9	7.5	-1.4
Fuel Gas Compressor Skid #1	320	43.8	57.1	54.8	47.1	44.1	40.1	35.2	36.5	34.0	30.2
Fuel Gas Compressor Skid #2	320	43.8	57.1	54.8	47.1	44.1	40.1	35.2	36.5	34.0	30.2
Tempering Air Fans #1	980	25.0	41.3	39.1	34.8	28.4	21.8	16.7	2.5	-6.8	-13.7
Tempering Air Fans #2	860	26.3	42.5	40.3	36.0	29.7	23.2	18.2	4.3	-4.4	-10.5
Distance to acoustic center	Near field										
CTG #1 Enclosure	990										
Standard Lw			120	110	113	106	100	95	92	92	85
Distance Correction			58	58	58	58	58	58	58	58	58
Atmospheric Absorption (59 deg F, 70% RH)			0	0	1	1	2	3	5	11	18
Directivity			0	0	0	0	0	0	0	0	0
Barrier			7	7	9	11	13	16	20	20	20
<b>CTG #1 Enclosure, SPL</b>		<b>33</b>	<b>55</b>	<b>45</b>	<b>46</b>	<b>36</b>	<b>28</b>	<b>18</b>	<b>9</b>	<b>4</b>	<b>-10</b>
CTG #1 Inlet Air Filter House	990										
Standard Lw			99	107	102	100	88	83	82	90	90
Distance Correction			58	58	58	58	58	58	58	58	58
Atmospheric Absorption (59 deg F, 70% RH)			0	0	1	1	2	3	5	10	18



Directivity			0	0	0	0	0	0	0	0	0
Barrier			6	6	8	10	11	14	17	20	20
<b>CTG #1 Inlet Air Filter House, SPL</b>		<b>26</b>	<b>35</b>	<b>43</b>	<b>36</b>	<b>31</b>	<b>18</b>	<b>9</b>	<b>2</b>	<b>2</b>	<b>-5</b>
SCR #1 Main Duct	990										
Standard Lw			118	112	104	101	91	81	77	78	80
Distance Correction			58	58	58	58	58	58	58	58	58
Atmospheric Absorption (59 deg F, 70% RH)			0	0	1	1	2	3	5	10	18
Directivity			0	0	0	0	0	0	0	0	0
Barrier			6	7	9	10	12	15	19	20	20
<b>SCR #1 Main Duct, SPL</b>		<b>27</b>	<b>54</b>	<b>47</b>	<b>37</b>	<b>32</b>	<b>20</b>	<b>6</b>	<b>-5</b>	<b>-10</b>	<b>-15</b>
SCR #1 Stack	990										
Standard Lw			123	120	107	96	85	80	77	77	79
Distance Correction			58	58	58	58	58	58	58	58	58
Atmospheric Absorption (59 deg F, 70% RH)			0	0	1	1	2	3	5	10	18
Directivity			0	0	0	0	0	0	0	0	0
Barrier			5	5	5	6	7	9	11	14	17
<b>SCR #1 Stack, SPL</b>		<b>33</b>	<b>60</b>	<b>57</b>	<b>44</b>	<b>31</b>	<b>19</b>	<b>11</b>	<b>3</b>	<b>-5</b>	<b>-13</b>
CTG #2 Enclosure	850										
Standard Lw			120	110	113	106	100	95	92	92	85
Distance Correction			56	56	56	56	56	56	56	56	56
Atmospheric Absorption (59 deg F, 70% RH)			0	0	1	1	2	3	4	9	15
Directivity			0	0	0	0	0	0	0	0	0
Barrier			7	7	9	11	13	16	20	20	20
<b>CTG #2 Enclosure, SPL</b>		<b>34</b>	<b>57</b>	<b>46</b>	<b>47</b>	<b>38</b>	<b>29</b>	<b>20</b>	<b>11</b>	<b>7</b>	<b>-6</b>
CTG #2 Inlet Air Filter House	850										
Standard Lw			99	107	102	100	88	83	82	90	90
Distance Correction			56	56	56	56	56	56	56	56	56
Atmospheric Absorption (59 deg F, 70% RH)			0	0	1	1	2	3	4	9	15
Directivity			0	0	0	0	0	0	0	0	0
Barrier			6	6	8	10	11	14	17	20	20
<b>CTG #2 Inlet Air Filter House, SPL</b>		<b>27</b>	<b>37</b>	<b>44</b>	<b>37</b>	<b>33</b>	<b>19</b>	<b>10</b>	<b>4</b>	<b>5</b>	<b>-1</b>
SCR #2 Main Duct	860										
Standard Lw			118	112	104	101	91	81	77	78	80
Distance Correction			56	56	56	56	56	56	56	56	56
Atmospheric Absorption (59 deg F, 70% RH)			0	0	1	1	2	3	4	9	15
Directivity			0	0	0	0	0	0	0	0	0
Barrier			6	7	9	10	12	15	19	20	20

[illegible]

Fuel Gas Compressor Skid #1	320										
Standard Lw			113	113	107	107	105	104	106	105	104
Distance Correction			48	48	48	48	48	48	48	48	48
Atmospheric Absorption (59 deg F, 70% RH)			0	0	0	0	1	1	2	3	6
Directivity			0	0	0	0	0	0	0	0	0
Barrier			8	10	12	15	17	20	20	20	20
<b>Fuel Gas Compressor Skid #1, SPL</b>		<b>44</b>	<b>57</b>	<b>55</b>	<b>47</b>	<b>44</b>	<b>40</b>	<b>35</b>	<b>37</b>	<b>34</b>	<b>30</b>
Fuel Gas Compressor Skid #2	320										
Standard Lw			113	113	107	107	105	104	106	105	104
Distance Correction			48	48	48	48	48	48	48	48	48
Atmospheric Absorption (59 deg F, 70% RH)			0	0	0	0	1	1	2	3	6
Directivity			0	0	0	0	0	0	0	0	0
Barrier			8	10	12	15	17	20	20	20	20
<b>Fuel Gas Compressor Skid #2, SPL</b>		<b>44</b>	<b>57</b>	<b>55</b>	<b>47</b>	<b>44</b>	<b>40</b>	<b>35</b>	<b>37</b>	<b>34</b>	<b>30</b>
Tempering Air Fans #1	980										
Standard Lw			106	104	102	98	94	93	85	81	81
Distance Correction			57	57	57	57	57	57	57	57	57
Atmospheric Absorption (59 deg F, 70% RH)			0	0	1	1	2	3	5	10	17
Directivity			0	0	0	0	0	0	0	0	0
Barrier			7	7	9	11	13	16	20	20	20
<b>Tempering Air Fans #1, SPL</b>		<b>25</b>	<b>41</b>	<b>39</b>	<b>35</b>	<b>28</b>	<b>22</b>	<b>17</b>	<b>3</b>	<b>-7</b>	<b>-14</b>
Tempering Air Fans #2	860										
Standard Lw			106	104	102	98	94	93	85	81	81
Distance Correction			56	56	56	56	56	56	56	56	56
Atmospheric Absorption (59 deg F, 70% RH)			0	0	1	1	2	3	4	9	15
Directivity			0	0	0	0	0	0	0	0	0
Barrier			7	7	9	11	13	16	20	20	20
<b>Tempering Air Fans #2, SPL</b>		<b>26</b>	<b>42</b>	<b>40</b>	<b>36</b>	<b>30</b>	<b>23</b>	<b>18</b>	<b>4</b>	<b>-4</b>	<b>-10</b>

Riverside Energy Resource Center

Sound Level Calculation

Nearest Industrial Property: 620 Feet South of Nominal Acoustic Center

	Distance (feet)	dBA	OCTAVE BAND CENTER FREQUENCY (Hz)								
			31.5	63	125	250	500	1000	2000	1220	8000
Receptor Location	Varies		77.7	72.9	67.1	62.8	56.7	51.7	49.8	45.9	37.3
		60.0	38.3	46.7	51.0	54.2	53.5	51.7	51.0	46.9	36.2
Summary											
CTG, CTG Auxiliary Skid, SCR, Exhaust Stk #1	440	53.6	75.4	70.3	63.2	57.0	48.7	43.2	39.3	38.9	33.8
CTG, CTG Auxiliary Skid, SCR, Exhaust Stk #2	560	51.3	73.3	68.2	61.0	54.8	46.4	40.8	36.5	35.5	29.5
Ammonia Evaporation Skid #1	455	48.7	54.1	54.0	53.9	51.7	47.4	41.9	34.9	28.4	20.2
Ammonia Evaporation Skid #2	575	46.4	52.0	51.9	51.7	49.5	45.2	39.5	32.2	25.1	16.1
Chiller Package	480	50.6	38.6	38.5	37.4	43.2	42.9	43.3	46.3	42.7	25.3
Auxiliary Cooling Tower	480	53.6	59.6	59.5	60.4	58.2	51.9	43.3	38.3	33.7	29.3
Fuel Gas Compressor Skid #1	1,145	47.6	53.8	53.3	47.4	47.1	44.6	41.6	41.2	34.2	24.5
Fuel Gas Compressor Skid #2	1,145	47.6	53.8	53.3	47.4	47.1	44.6	41.6	41.2	34.2	24.5
Tempering Air Fans #1	460	45.1	55.0	52.9	50.8	46.6	42.3	40.8	31.8	25.3	22.0
Tempering Air Fans #2	580	42.8	53.0	50.9	48.7	44.5	40.1	38.4	29.1	22.0	17.9
Distance to acoustic center	Near field										
CTG, CTG Auxiliary Skid, SCR, Exhaust Stack #1	440										
Standard Lw			126	121	114	108	100	95	92	94	92
Distance Correction			50	50	50	50	50	50	50	50	50
Atmospheric Absorption (59 deg F, 70% RH)			0	0	0	1	1	1	2	5	8
Directivity			0	0	0	0	0	0	0	0	0
<b>CTG Unit #1, SPL</b>		<b>54</b>	<b>75</b>	<b>70</b>	<b>63</b>	<b>57</b>	<b>49</b>	<b>43</b>	<b>39</b>	<b>39</b>	<b>34</b>
CTG, CTG Auxiliary Skid, SCR, Exhaust Stack #2	560										
Standard Lw			126	121	114	108	100	95	92	94	92
Distance Correction			53	53	53	53	53	53	53	53	53
Atmospheric Absorption (59 deg F, 70% RH)			0	0	0	1	1	2	3	6	10
Directivity			0	0	0	0	0	0	0	0	0
<b>CTG Unit #2, SPL</b>		<b>51</b>	<b>73</b>	<b>68</b>	<b>61</b>	<b>55</b>	<b>46</b>	<b>41</b>	<b>37</b>	<b>36</b>	<b>30</b>
Ammonia Evaporation Skid #1	455										
Standard Lw			105	105	105	103	99	94	88	84	79
Distance Correction			51	51	51	51	51	51	51	51	51
Atmospheric Absorption (59 deg F, 70% RH)			0	0	0	1	1	1	2	5	8

Directivity			0	0	0	0	0	0	0	0	0
<b>Ammonia Evaporation Skid #1, SPL</b>		<b>49</b>	<b>54</b>	<b>54</b>	<b>54</b>	<b>52</b>	<b>47</b>	<b>42</b>	<b>35</b>	<b>28</b>	<b>20</b>
Ammonia Evaporation Skid #2	575										
Standard Lw			105	105	105	103	99	94	88	84	79
Distance Correction			53	53	53	53	53	53	53	53	53
Atmospheric Absorption (59 deg F, 70% RH)			0	0	0	1	1	2	3	6	10
Directivity			0	0	0	0	0	0	0	0	0
<b>Ammonia Evaporation Skid #2, SPL</b>		<b>46</b>	<b>52</b>	<b>52</b>	<b>52</b>	<b>50</b>	<b>45</b>	<b>39</b>	<b>32</b>	<b>25</b>	<b>16</b>
Chiller Package	480										
Standard Lw			90	90	89	95	95	96	100	99	85
Distance Correction			51	51	51	51	51	51	51	51	51
Atmospheric Absorption (59 deg F, 70% RH)			0	0	0	1	1	1	2	5	8
Directivity			0	0	0	0	0	0	0	0	0
<b>Chiller Package, SPL</b>		<b>51</b>	<b>39</b>	<b>39</b>	<b>37</b>	<b>43</b>	<b>43</b>	<b>43</b>	<b>46</b>	<b>43</b>	<b>25</b>
Auxiliary Cooling Tower	480										
Standard Lw			111	111	112	110	104	96	92	90	89
Distance Correction			51	51	51	51	51	51	51	51	51
Atmospheric Absorption (59 deg F, 70% RH)			0	0	0	1	1	1	2	5	8
Directivity			0	0	0	0	0	0	0	0	0
<b>Auxiliary Cooling Tower, SPL</b>		<b>54</b>	<b>60</b>	<b>60</b>	<b>60</b>	<b>58</b>	<b>52</b>	<b>43</b>	<b>38</b>	<b>34</b>	<b>29</b>
Fuel Gas Compressor Skid #1	1,145										
Standard Lw			113	113	107	107	105	104	106	105	104
Distance Correction			59	59	59	59	59	59	59	59	59
Atmospheric Absorption (59 deg F, 70% RH)			0	1	1	1	2	3	6	12	20
Directivity			0	0	0	0	0	0	0	0	0
<b>Fuel Gas Compressor Skid #1, SPL</b>		<b>48</b>	<b>54</b>	<b>53</b>	<b>47</b>	<b>47</b>	<b>45</b>	<b>42</b>	<b>41</b>	<b>34</b>	<b>24</b>
Fuel Gas Compressor Skid #2	1,145										
Standard Lw			113	113	107	107	105	104	106	105	104
Distance Correction			59	59	59	59	59	59	59	59	59
Atmospheric Absorption (59 deg F, 70% RH)			0	1	1	1	2	3	6	12	20
Directivity			0	0	0	0	0	0	0	0	0
<b>Fuel Gas Compressor Skid #2, SPL</b>		<b>48</b>	<b>54</b>	<b>53</b>	<b>47</b>	<b>47</b>	<b>45</b>	<b>42</b>	<b>41</b>	<b>34</b>	<b>24</b>
Tempering Air Fans #1	460										
Standard Lw			106	104	102	98	94	93	85	81	81
Distance Correction			51	51	51	51	51	51	51	51	51
Atmospheric Absorption (59 deg F, 70% RH)			0	0	0	1	1	1	2	5	8

Directivity			0	0	0	0	0	0	0	0	0
<b>Tempering Air Fans #1, SPL</b>		<b>45</b>	<b>55</b>	<b>53</b>	<b>51</b>	<b>47</b>	<b>42</b>	<b>41</b>	<b>32</b>	<b>25</b>	<b>22</b>
Tempering Air Fans #2	580										
Standard Lw			106	104	102	98	94	93	85	81	81
Distance Correction			53	53	53	53	53	53	53	53	53
Atmospheric Absorption (59 deg F, 70% RH)			0	0	0	1	1	2	3	6	10
Directivity			0	0	0	0	0	0	0	0	0
<b>Tempering Air Fans #2, SPL</b>		<b>43</b>	<b>53</b>	<b>51</b>	<b>49</b>	<b>44</b>	<b>40</b>	<b>38</b>	<b>29</b>	<b>22</b>	<b>18</b>

Riverside Energy Resource Center

Sound Level Calculation

Nearest Industrial Property: 330 Feet East of Nominal Acoustic Center

	Distance (feet)	dBA	OCTAVE BAND CENTER FREQUENCY (Hz)								
			31.5	63	125	250	500	1000	2000	1220	8000
Receptor Location	Varies		74.6	69.9	64.3	60.3	54.5	49.7	48.2	43.0	33.1
		57.7	35.2	43.7	48.2	51.7	51.3	49.7	49.4	44.0	32.0
Summary											
CTG, CTG Auxiliary Skid, SCR, Exhaust Stk #1	670	49.5	71.7	66.6	59.3	53.1	44.7	38.9	34.4	32.8	26.0
CTG, CTG Auxiliary Skid, SCR, Exhaust Stk #2	720	48.8	71.0	65.9	58.7	52.4	44.0	38.1	33.5	31.6	24.5
Ammonia Evaporation Skid #1	630	45.5	51.2	51.1	50.9	48.7	44.3	38.5	31.2	23.8	14.3
Ammonia Evaporation Skid #2	690	44.6	50.4	50.3	50.1	47.8	43.4	37.6	30.1	22.3	12.4
Chiller Package	620	47.6	36.4	36.2	35.0	40.8	40.4	40.7	43.3	39.0	20.6
Auxiliary Cooling Tower	620	51.1	57.4	57.2	58.0	55.8	49.4	40.7	35.3	30.0	24.6
Fuel Gas Compressor Skid #1	1,070	48.5	54.4	53.9	48.0	47.8	45.3	42.4	42.2	35.6	26.4
Fuel Gas Compressor Skid #2	1,070	48.5	54.4	53.9	48.0	47.8	45.3	42.4	42.2	35.6	26.4
Tempering Air Fans #1	680	41.2	51.6	49.4	47.2	43.0	38.5	36.7	27.2	19.6	14.7
Tempering Air Fans #2	720	40.6	51.0	48.9	46.7	42.4	38.0	36.1	26.5	18.6	13.5
Distance to acoustic center	Near field										
CTG, CTG Auxiliary Skid, SCR, Exhaust Stack #1	670										
Standard Lw			126	121	114	108	100	95	92	94	92
Distance Correction			54	54	54	54	54	54	54	54	54
Atmospheric Absorption (59 deg F, 70% RH)			0	0	1	1	1	2	3	7	12
Directivity			0	0	0	0	0	0	0	0	0
<b>CTG Unit #1, SPL</b>		<b>50</b>	<b>72</b>	<b>67</b>	<b>59</b>	<b>53</b>	<b>45</b>	<b>39</b>	<b>34</b>	<b>33</b>	<b>26</b>
CTG, CTG Auxiliary Skid, SCR, Exhaust Stack #2	720										
Standard Lw			126	121	114	108	100	95	92	94	92
Distance Correction			55	55	55	55	55	55	55	55	55
Atmospheric Absorption (59 deg F, 70% RH)			0	0	1	1	1	2	4	8	13
Directivity			0	0	0	0	0	0	0	0	0
<b>CTG Unit #2, SPL</b>		<b>49</b>	<b>71</b>	<b>66</b>	<b>59</b>	<b>52</b>	<b>44</b>	<b>38</b>	<b>34</b>	<b>32</b>	<b>25</b>
Ammonia Evaporation Skid #1	630										
Standard Lw			105	105	105	103	99	94	88	84	79
Distance Correction			54	54	54	54	54	54	54	54	54
Atmospheric Absorption (59 deg F, 70% RH)			0	0	1	1	1	2	3	7	11

Directivity			0	0	0	0	0	0	0	0	0
<b>Ammonia Evaporation Skid #1, SPL</b>		<b>46</b>	<b>51</b>	<b>51</b>	<b>51</b>	<b>49</b>	<b>44</b>	<b>39</b>	<b>31</b>	<b>24</b>	<b>14</b>
Ammonia Evaporation Skid #2	690										
Standard Lw			105	105	105	103	99	94	88	84	79
Distance Correction			54	54	54	54	54	54	54	54	54
Atmospheric Absorption (59 deg F, 70% RH)			0	0	1	1	1	2	4	7	12
Directivity			0	0	0	0	0	0	0	0	0
<b>Ammonia Evaporation Skid #2, SPL</b>		<b>45</b>	<b>50</b>	<b>50</b>	<b>50</b>	<b>48</b>	<b>43</b>	<b>38</b>	<b>30</b>	<b>22</b>	<b>12</b>
Chiller Package	620										
Standard Lw			90	90	89	95	95	96	100	99	85
Distance Correction			53	53	53	53	53	53	53	53	53
Atmospheric Absorption (59 deg F, 70% RH)			0	0	1	1	1	2	3	7	11
Directivity			0	0	0	0	0	0	0	0	0
<b>Chiller Package, SPL</b>		<b>48</b>	<b>36</b>	<b>36</b>	<b>35</b>	<b>41</b>	<b>40</b>	<b>41</b>	<b>43</b>	<b>39</b>	<b>21</b>
Auxiliary Cooling Tower	620										
Standard Lw			111	111	112	110	104	96	92	90	89
Distance Correction			53	53	53	53	53	53	53	53	53
Atmospheric Absorption (59 deg F, 70% RH)			0	0	1	1	1	2	3	7	11
Directivity			0	0	0	0	0	0	0	0	0
<b>Auxiliary Cooling Tower, SPL</b>		<b>51</b>	<b>57</b>	<b>57</b>	<b>58</b>	<b>56</b>	<b>49</b>	<b>41</b>	<b>35</b>	<b>30</b>	<b>25</b>
Fuel Gas Compressor Skid #1	1,070										
Standard Lw			113	113	107	107	105	104	106	105	104
Distance Correction			58	58	58	58	58	58	58	58	58
Atmospheric Absorption (59 deg F, 70% RH)			0	1	1	1	2	3	6	11	19
Directivity			0	0	0	0	0	0	0	0	0
<b>Fuel Gas Compressor Skid #1, SPL</b>		<b>48</b>	<b>54</b>	<b>54</b>	<b>48</b>	<b>48</b>	<b>45</b>	<b>42</b>	<b>42</b>	<b>36</b>	<b>26</b>
Fuel Gas Compressor Skid #2	1,070										
Standard Lw			113	113	107	107	105	104	106	105	104
Distance Correction			58	58	58	58	58	58	58	58	58
Atmospheric Absorption (59 deg F, 70% RH)			0	1	1	1	2	3	6	11	19
Directivity			0	0	0	0	0	0	0	0	0
<b>Fuel Gas Compressor Skid #2, SPL</b>		<b>48</b>	<b>54</b>	<b>54</b>	<b>48</b>	<b>48</b>	<b>45</b>	<b>42</b>	<b>42</b>	<b>36</b>	<b>26</b>
Tempering Air Fans #1	680										
Standard Lw			106	104	102	98	94	93	85	81	81
Distance Correction			54	54	54	54	54	54	54	54	54
Atmospheric Absorption (59 deg F, 70% RH)			0	0	1	1	1	2	4	7	12



Directivity			0	0	0	0	0	0	0	0	0
<b>Tempering Air Fans #1, SPL</b>		<b>41</b>	<b>52</b>	<b>49</b>	<b>47</b>	<b>43</b>	<b>39</b>	<b>37</b>	<b>27</b>	<b>20</b>	<b>15</b>
Tempering Air Fans #2	720										
Standard Lw			106	104	102	98	94	93	85	81	81
Distance Correction			55	55	55	55	55	55	55	55	55
Atmospheric Absorption (59 deg F, 70% RH)			0	0	1	1	1	2	4	8	13
Directivity			0	0	0	0	0	0	0	0	0
<b>Tempering Air Fans #2, SPL</b>		<b>41</b>	<b>51</b>	<b>49</b>	<b>47</b>	<b>42</b>	<b>38</b>	<b>36</b>	<b>27</b>	<b>19</b>	<b>14</b>

Riverside Energy Resource Center

Sound Level Calculation

Nearest Office Property: 690 Feet West of Nominal Acoustic Center

	Distance (feet)	dBA	OCTAVE BAND CENTER FREQUENCY (Hz)								
			31.5	63	125	250	500	1000	2000	1220	8000
Receptor Location	Varies		73.8	68.9	62.9	58.3	52.1	47.0	44.6	39.3	29.8
		55.3	34.4	42.7	46.7	49.6	48.7	46.7	45.7	40.3	28.6
Summary											
CTG, CTG Auxiliary Skid, SCR, Exhaust Stk #1	760	48.3	70.6	65.4	58.2	51.9	43.4	37.5	32.9	30.8	23.4
CTG, CTG Auxiliary Skid, SCR, Exhaust Stk #2	750	48.4	70.7	65.5	58.3	52.0	43.6	37.7	33.0	31.0	23.7
Ammonia Evaporation Skid #1	800	43.1	49.1	49.0	48.7	46.4	41.9	36.0	28.2	19.9	9.2
Ammonia Evaporation Skid #2	810	43.0	49.0	48.8	48.6	46.3	41.8	35.8	28.0	19.7	8.9
Chiller Package	830	44.0	33.8	33.6	32.3	38.0	37.5	37.5	39.7	34.2	14.3
Auxiliary Cooling Tower	830	48.2	54.8	54.6	55.3	53.0	46.5	37.5	31.7	25.2	18.3
Fuel Gas Compressor Skid #1	1,030	44.0	49.7	49.3	43.4	43.1	40.7	37.9	37.7	31.4	22.4
Fuel Gas Compressor Skid #2	1,030	44.0	49.7	49.3	43.4	43.1	40.7	37.9	37.7	31.4	22.4
Tempering Air Fans #1	760	40.1	50.6	48.4	46.2	41.9	37.4	35.5	25.9	17.8	12.4
Tempering Air Fans #2	760	40.1	50.6	48.4	46.2	41.9	37.4	35.5	25.9	17.8	12.4
Distance to acoustic center	Near field										
CTG, CTG Auxiliary Skid, SCR, Exhaust Stack #1	760										
Standard Lw			126	121	114	108	100	95	92	94	92
Distance Correction			55	55	55	55	55	55	55	55	55
Atmospheric Absorption (59 deg F, 70% RH)			0	0	1	1	1	2	4	8	13
Directivity			0	0	0	0	0	0	0	0	0
CTG Unit #1, SPL		48	71	65	58	52	43	38	33	31	23
CTG, CTG Auxiliary Skid, SCR, Exhaust Stack #2	750										
Standard Lw			126	121	114	108	100	95	92	94	92
Distance Correction			55	55	55	55	55	55	55	55	55
Atmospheric Absorption (59 deg F, 70% RH)			0	0	1	1	1	2	4	8	13
Directivity			0	0	0	0	0	0	0	0	0
CTG Unit #2, SPL		48	71	66	58	52	44	38	33	31	24
Ammonia Evaporation Skid #1	800										
Standard Lw			105	105	105	103	99	94	88	84	79
Distance Correction			56	56	56	56	56	56	56	56	56
Atmospheric Absorption (59 deg F, 70% RH)			0	0	1	1	1	2	4	8	14

Directivity			0	0	0	0	0	0	0	0	0
<b>Ammonia Evaporation Skid #1, SPL</b>		<b>43</b>	<b>49</b>	<b>49</b>	<b>49</b>	<b>46</b>	<b>42</b>	<b>36</b>	<b>28</b>	<b>20</b>	<b>9</b>
Ammonia Evaporation Skid #2	810										
Standard Lw			105	105	105	103	99	94	88	84	79
Distance Correction			56	56	56	56	56	56	56	56	56
Atmospheric Absorption (59 deg F, 70% RH)			0	0	1	1	1	2	4	9	14
Directivity			0	0	0	0	0	0	0	0	0
<b>Ammonia Evaporation Skid #2, SPL</b>		<b>43</b>	<b>49</b>	<b>49</b>	<b>49</b>	<b>46</b>	<b>42</b>	<b>36</b>	<b>28</b>	<b>20</b>	<b>9</b>
Chiller Package	830										
Standard Lw			90	90	89	95	95	96	100	99	85
Distance Correction			56	56	56	56	56	56	56	56	56
Atmospheric Absorption (59 deg F, 70% RH)			0	0	1	1	1	2	4	9	15
Directivity			0	0	0	0	0	0	0	0	0
<b>Chiller Package, SPL</b>		<b>44</b>	<b>34</b>	<b>34</b>	<b>32</b>	<b>38</b>	<b>38</b>	<b>38</b>	<b>40</b>	<b>34</b>	<b>14</b>
Auxiliary Cooling Tower	830										
Standard Lw			111	111	112	110	104	96	92	90	89
Distance Correction			56	56	56	56	56	56	56	56	56
Atmospheric Absorption (59 deg F, 70% RH)			0	0	1	1	1	2	4	9	15
Directivity			0	0	0	0	0	0	0	0	0
<b>Auxiliary Cooling Tower, SPL</b>		<b>48</b>	<b>55</b>	<b>55</b>	<b>55</b>	<b>53</b>	<b>47</b>	<b>38</b>	<b>32</b>	<b>25</b>	<b>18</b>
Fuel Gas Compressor Skid #1	1,030										
Standard Lw			113	113	107	107	105	104	106	105	104
Distance Correction			58	58	58	58	58	58	58	58	58
Atmospheric Absorption (59 deg F, 70% RH)			0	1	1	1	2	3	5	11	18
14' Sound-Absorptive Barrier			5	5	5	5	5	5	5	5	5
Directivity			0	0	0	0	0	0	0	0	0
<b>Fuel Gas Compressor Skid #1, SPL</b>		<b>44</b>	<b>50</b>	<b>49</b>	<b>43</b>	<b>43</b>	<b>41</b>	<b>38</b>	<b>38</b>	<b>31</b>	<b>22</b>
Fuel Gas Compressor Skid #2	1,030										
Standard Lw			113	113	107	107	105	104	106	105	104
Distance Correction			58	58	58	58	58	58	58	58	58
Atmospheric Absorption (59 deg F, 70% RH)			0	1	1	1	2	3	5	11	18
14' Sound-Absorptive Barrier			5	5	5	5	5	5	5	5	5
Directivity			0	0	0	0	0	0	0	0	0
<b>Fuel Gas Compressor Skid #2, SPL</b>		<b>44</b>	<b>50</b>	<b>49</b>	<b>43</b>	<b>43</b>	<b>41</b>	<b>38</b>	<b>38</b>	<b>31</b>	<b>22</b>
Tempering Air Fans #1	760										
Standard Lw			106	104	102	98	94	93	85	81	81

Distance Correction			55	55	55	55	55	55	55	55	55
Atmospheric Absorption (59 deg F, 70% RH)			0	0	1	1	1	2	4	8	13
Directivity			0	0	0	0	0	0	0	0	0
<b>Tempering Air Fans #1, SPL</b>		<b>40</b>	<b>51</b>	<b>48</b>	<b>46</b>	<b>42</b>	<b>37</b>	<b>36</b>	<b>26</b>	<b>18</b>	<b>12</b>
Tempering Air Fans #2	760										
Standard Lw			106	104	102	98	94	93	85	81	81
Distance Correction			55	55	55	55	55	55	55	55	55
Atmospheric Absorption (59 deg F, 70% RH)			0	0	1	1	1	2	4	8	13
Directivity			0	0	0	0	0	0	0	0	0
<b>Tempering Air Fans #2, SPL</b>		<b>40</b>	<b>51</b>	<b>48</b>	<b>46</b>	<b>42</b>	<b>37</b>	<b>36</b>	<b>26</b>	<b>18</b>	<b>12</b>

### Sound Level Calculation

**Nearest Industrial Property: 2,320 Feet North of Nominal Acoustic Center**

[illegible]

Standard Lw			111	111	112	110	104	96	92	90	89
Distance Correction			65	65	65	65	65	65	65	65	65
Atmospheric Absorption (59 deg F, 70% RH)			1	1	2	3	4	7	12	25	41
Directivity			0	0	0	0	0	0	0	0	0
<b>Auxiliary Cooling Tower, SPL</b>		<b>37</b>	<b>45</b>	<b>45</b>	<b>45</b>	<b>42</b>	<b>35</b>	<b>24</b>	<b>15</b>	<b>1</b>	<b>-17</b>
Fuel Gas Compressor Skid	2,320										
Standard Lw			116	116	110	110	108	107	109	108	107
Distance Correction			65	65	65	65	65	65	65	65	65
Atmospheric Absorption (59 deg F, 70% RH)			1	1	2	3	4	7	12	25	41
Directivity			0	0	0	0	0	0	0	0	0
<b>Fuel Gas Compressor Skid, SPL</b>		<b>41</b>	<b>50</b>	<b>50</b>	<b>43</b>	<b>43</b>	<b>39</b>	<b>35</b>	<b>32</b>	<b>19</b>	<b>1</b>
Tempering Air Fans	2,320										
Standard Lw			109	107	105	101	97	96	88	84	84
Distance Correction			65	65	65	65	65	65	65	65	65
Atmospheric Absorption (59 deg F, 70% RH)			1	1	2	3	4	7	12	25	41
Directivity			0	0	0	0	0	0	0	0	0
<b>Tempering Air Fans, SPL</b>		<b>30</b>	<b>43</b>	<b>41</b>	<b>38</b>	<b>33</b>	<b>28</b>	<b>24</b>	<b>11</b>	<b>-5</b>	<b>-22</b>

# **CURE Data Requests Set 3**

## **Noise - Attachment 6**

C:\LARDAV\SLMUTIL\15F31603.bin Interval Data

Date	Time	Duration	Leq	Lmax	Lmin	L( 2)	L(10)	L(25)	L(50)	L(90)	L(99)	Over loads
15Mar 04	14:36:11	1428.1	72.4	93.2	44.9	86.0	58.2	52.2	49.7	47.2	45.7	0
15Mar 04	15:00:00	3600.0	71.4	92.6	44.2	82.4	58.4	51.3	48.7	46.3	45.1	0
15Mar 04	16:00:00	3600.0	64.6	89.8	44.2	73.4	56.9	51.2	48.8	46.3	44.8	0
15Mar 04	17:00:00	3600.0	65.8	89.2	45.4	73.7	59.8	54.5	51.5	48.3	46.4	0
15Mar 04	18:00:00	3600.0	69.1	92.1	44.8	79.9	55.9	51.9	50.4	46.9	45.3	0
15Mar 04	19:00:00	3600.0	65.4	90.2	44.4	73.8	56.1	52.7	50.7	46.8	45.3	0
15Mar 04	20:00:00	3600.0	67.9	90.1	44.0	77.1	66.1	52.7	47.9	45.3	44.2	0
15Mar 04	21:00:00	3600.0	64.9	89.6	43.3	73.1	51.2	48.8	46.9	44.6	43.5	0
15Mar 04	22:00:00	3600.0	69.9	92.9	44.4	80.8	67.7	53.0	50.0	46.2	44.9	0
15Mar 04	23:00:00	3600.0	70.5	95.6	42.4	80.2	53.8	51.1	48.0	44.6	43.1	0
16Mar 04	00:00:00	3600.0	46.1	57.3	41.7	51.5	47.8	46.3	45.1	43.3	42.1	0
16Mar 04	01:00:00	3600.0	67.3	86.6	41.2	79.8	54.8	47.3	45.5	43.1	41.8	0
16Mar 04	02:00:00	3600.0	66.7	91.8	40.5	77.6	47.7	45.3	43.9	41.6	40.5	0
16Mar 04	03:00:00	3600.0	45.0	64.4	41.0	47.8	45.8	45.0	44.3	42.6	41.5	0
16Mar 04	04:00:00	3600.0	72.0	94.6	44.5	82.0	58.1	49.2	47.8	46.1	45.0	0
16Mar 04	05:00:00	3600.0	71.2	94.8	45.0	73.0	54.8	52.4	50.4	47.0	46.0	0
16Mar 04	06:00:00	3600.0	67.9	92.0	49.0	77.0	56.6	53.6	52.1	50.2	49.2	0
16Mar 04	07:00:00	3600.0	68.6	92.5	48.7	78.2	56.0	53.4	52.1	50.3	49.2	0
16Mar 04	08:00:00	3600.0	64.2	89.7	47.2	70.8	61.2	53.9	52.0	49.8	48.3	0
16Mar 04	09:00:00	3600.0	68.9	93.1	42.2	80.5	53.4	50.9	48.8	45.7	43.8	0
16Mar 04	10:00:00	3600.0	67.1	91.7	42.0	75.8	54.0	50.6	48.5	45.3	43.5	0
16Mar 04	11:00:00	3600.0	64.1	94.0	42.4	60.6	54.6	52.5	50.4	47.1	44.5	0
16Mar 04	12:00:00	3600.0	71.2	93.6	43.5	81.1	71.2	53.9	50.7	47.2	44.7	0
16Mar 04	13:00:00	3600.0	70.1	95.3	40.6	78.3	57.2	50.7	47.2	43.6	41.8	0
16Mar 04	14:00:00	3600.0	57.3	84.4	39.2	59.4	52.6	48.7	45.9	42.7	40.4	0
16Mar 04	15:00:00	3600.0	70.2	95.8	38.5	79.1	52.8	47.0	44.3	41.5	39.7	0
16Mar 04	16:00:00	820.8	49.6	64.5	40.5	58.8	52.6	46.3	44.0	42.2	41.1	0



C:\LARDAV\SLMUTIL\5FT31601.bin Interval Data

Date	Time	Duration	Leq	Lmax	Lmin	L( 2)	L(10)	L(25)	L(50)	L(90)	L(99)	Over loads
15Mar 04	14:36:49	1390.8	64.0	84.5	40.1	77.0	57.3	48.9	45.5	42.7	41.3	0
15Mar 04	15:00:00	3600.0	63.5	85.9	38.7	73.6	56.3	47.5	44.4	41.5	39.7	0
15Mar 04	16:00:00	3600.0	57.9	83.6	38.8	65.8	54.8	48.1	44.7	41.5	39.7	0
15Mar 04	17:00:00	3600.0	59.1	84.9	40.5	66.5	56.4	51.4	47.1	43.4	41.6	0
15Mar 04	18:00:00	3600.0	61.5	87.1	38.4	70.2	50.1	45.7	43.9	41.1	39.4	0
15Mar 04	19:00:00	3600.0	56.4	82.6	38.5	64.4	51.0	46.3	44.1	40.8	39.2	0
15Mar 04	20:00:00	3600.0	61.5	85.4	38.5	68.4	57.5	45.6	42.6	40.0	39.0	0
15Mar 04	21:00:00	3600.0	56.7	83.9	37.7	64.1	45.4	42.8	40.9	39.0	38.1	0
15Mar 04	22:00:00	3600.0	62.8	87.4	38.7	72.3	58.6	46.0	43.0	40.1	39.1	0
15Mar 04	23:00:00	3600.0	60.6	84.7	37.3	70.6	46.7	44.1	41.8	39.6	38.2	0
16Mar 04	00:00:00	3600.0	41.6	55.8	37.4	47.2	42.7	41.6	40.5	39.0	38.1	0
16Mar 04	01:00:00	3600.0	58.7	81.3	37.1	70.4	48.7	42.1	41.2	38.8	37.5	0
16Mar 04	02:00:00	3600.0	59.4	86.4	36.5	68.2	42.6	40.8	39.7	37.7	37.0	0
16Mar 04	03:00:00	3600.0	40.9	57.3	37.1	43.6	41.9	41.1	40.3	38.6	37.4	0
16Mar 04	04:00:00	3600.0	64.3	88.8	40.6	72.2	53.4	45.5	44.0	42.0	41.1	0
16Mar 04	05:00:00	3600.0	61.4	85.7	41.3	67.9	52.4	48.3	46.7	43.3	42.1	0
16Mar 04	06:00:00	3600.0	58.7	82.0	44.5	67.6	53.4	49.9	47.9	46.0	45.1	0
16Mar 04	07:00:00	3600.0	62.9	89.5	44.4	69.4	53.6	49.6	48.0	46.3	45.2	0
16Mar 04	08:00:00	3600.0	58.4	82.6	42.8	64.7	57.7	50.3	48.0	45.1	43.6	0
16Mar 04	09:00:00	3600.0	61.9	88.5	39.0	71.2	50.8	47.4	44.8	41.5	39.8	0
16Mar 04	10:00:00	3600.0	59.9	85.5	38.0	67.0	51.1	46.9	44.3	40.8	39.0	0
16Mar 04	11:00:00	3600.0	55.0	82.4	38.7	59.4	51.9	49.5	46.9	42.6	40.2	0
16Mar 04	12:00:00	3600.0	63.4	86.9	39.5	72.6	63.2	51.5	47.7	43.4	41.1	0
16Mar 04	13:00:00	3600.0	61.2	86.0	36.1	68.6	52.6	47.5	43.4	39.3	37.7	0
16Mar 04	14:00:00	3600.0	50.7	74.1	34.2	58.9	50.7	45.7	42.2	38.0	35.8	0
16Mar 04	15:00:00	3600.0	61.2	87.9	34.6	70.7	50.6	43.9	40.7	37.5	35.5	0
16Mar 04	16:00:00	851.2	49.0	71.9	37.3	58.7	50.7	42.8	40.5	38.5	37.3	0

## 5FTLT2.TXT

C:\LARDAV\SLMUTIL\5FT31702.bin Interval Data

Date	Time	Duration	Leq	Lmax	Lmin	L( 2)	L(10)	L(25)	L(50)	L(90)	L(99)	Over loads
16Mar 04	17:58:03	116.3	54.3	73.0	42.5	63.9	52.8	49.9	47.8	43.7	42.5	0
16Mar 04	18:00:00	3600.0	51.5	71.4	41.6	59.3	53.8	50.7	47.2	43.4	42.2	0
16Mar 04	19:00:00	3600.0	55.6	76.9	40.1	66.1	54.7	48.8	44.9	42.3	40.7	0
16Mar 04	20:00:00	3600.0	51.7	75.1	40.7	58.0	51.7	47.3	45.3	43.3	42.1	0
16Mar 04	21:00:00	3600.0	50.0	71.6	42.4	56.9	50.8	48.7	47.3	44.8	43.1	0
16Mar 04	22:00:00	3600.0	53.2	83.1	42.8	52.9	48.5	47.1	46.2	44.5	43.4	0
16Mar 04	23:00:00	3600.0	46.2	67.9	41.9	51.4	46.7	45.6	44.7	43.3	42.2	0
17Mar 04	00:00:00	3600.0	44.7	59.5	39.4	48.2	46.5	45.5	44.3	41.4	40.2	0
17Mar 04	01:00:00	3600.0	45.2	58.6	39.1	51.8	47.0	45.0	43.6	41.5	40.2	0
17Mar 04	02:00:00	3600.0	45.8	64.2	38.8	51.3	48.1	45.7	43.8	41.4	40.2	0
17Mar 04	03:00:00	3600.0	47.4	57.9	41.5	52.6	49.9	48.2	46.3	43.7	42.2	0
17Mar 04	04:00:00	3600.0	50.9	67.9	43.6	55.3	52.9	51.5	50.1	47.1	45.1	0
17Mar 04	05:00:00	3600.0	55.2	72.4	46.1	61.0	57.0	55.5	53.5	49.5	47.7	0
17Mar 04	06:00:00	3600.0	55.6	75.1	49.4	60.3	56.9	55.2	53.9	51.6	50.2	0
17Mar 04	07:00:00	3600.0	58.6	71.6	48.6	66.4	62.7	59.1	54.8	50.8	49.2	0
17Mar 04	08:00:00	3600.0	54.4	68.1	43.4	63.0	58.2	53.7	50.5	46.2	44.1	0
17Mar 04	09:00:00	3600.0	57.1	71.8	39.9	65.5	61.0	57.1	52.7	43.8	41.2	0
17Mar 04	10:00:00	3600.0	55.8	72.2	36.0	65.4	59.6	54.1	48.0	40.1	37.5	0
17Mar 04	11:00:00	3600.0	54.3	71.5	35.5	65.2	56.9	50.0	44.7	39.4	37.1	0
17Mar 04	12:00:00	3600.0	50.2	71.1	35.7	58.5	50.6	47.7	45.1	40.5	37.6	0
17Mar 04	13:00:00	3600.0	48.9	68.7	32.9	57.1	51.0	46.6	43.3	38.6	33.9	0
17Mar 04	14:00:00	3600.0	54.9	78.0	32.9	61.9	53.8	47.7	42.9	37.1	34.0	0
17Mar 04	15:00:00	3600.0	57.6	79.4	37.2	67.0	57.1	53.5	49.9	44.1	40.4	0
17Mar 04	16:00:00	3600.0	48.5	64.4	40.0	56.5	51.7	47.9	45.2	42.4	41.1	0
17Mar 04	17:00:00	3600.0	59.4	89.9	40.6	64.9	55.3	50.8	47.4	43.6	41.7	0
17Mar 04	18:00:00	3600.0	53.2	75.2	41.2	62.3	53.3	48.6	45.2	42.7	41.5	0
17Mar 04	19:00:00	279.9	50.1	64.0	40.8	61.1	50.4	44.8	43.2	41.7	41.0	0

C:\LARDAV\SLMUTIL\15F31702.bin Interval Data

Date	Time	Duration	Leq	Lmax	Lmin	L( 2)	L(10)	L(25)	L(50)	L(90)	L(99)	Over loads
16Mar 04	17:57:45	134.6	54.6	65.0	45.5	62.3	57.5	54.7	52.2	48.3	45.8	0
16Mar 04	18:00:00	3600.0	56.1	74.8	44.0	63.8	58.4	55.1	51.5	46.4	45.0	0
16Mar 04	19:00:00	3600.0	56.8	77.8	43.6	67.1	57.5	52.2	48.5	45.9	44.3	0
16Mar 04	20:00:00	3600.0	53.8	75.2	44.1	62.2	54.4	50.9	49.0	46.3	45.0	0
16Mar 04	21:00:00	3600.0	52.8	71.2	45.4	59.6	54.4	52.3	50.8	48.1	46.2	0
16Mar 04	22:00:00	3600.0	58.7	89.6	46.8	55.6	52.3	50.9	49.9	48.3	47.2	0
16Mar 04	23:00:00	3600.0	50.2	73.4	45.3	54.0	50.0	48.9	48.2	46.8	46.0	0
17Mar 04	00:00:00	3600.0	48.3	68.0	41.7	51.6	49.6	48.6	47.4	44.2	42.7	0
17Mar 04	01:00:00	3600.0	48.0	61.7	41.6	54.8	49.9	47.9	46.2	43.8	42.4	0
17Mar 04	02:00:00	3600.0	49.2	71.9	42.2	55.3	50.3	47.9	46.3	44.2	43.0	0
17Mar 04	03:00:00	3600.0	49.7	62.3	44.0	54.7	52.0	50.3	48.8	46.3	44.7	0
17Mar 04	04:00:00	3600.0	53.8	74.0	46.2	58.1	55.6	54.1	52.5	49.3	47.6	0
17Mar 04	05:00:00	3600.0	56.6	72.0	49.2	62.9	57.8	56.6	55.2	52.0	50.2	0
17Mar 04	06:00:00	3600.0	57.8	75.1	51.9	64.1	59.3	57.6	56.3	54.2	52.9	0
17Mar 04	07:00:00	3600.0	59.8	80.3	51.6	66.7	63.2	59.8	56.5	53.3	52.1	0
17Mar 04	08:00:00	3600.0	55.4	68.6	47.2	63.3	58.7	55.0	52.7	49.4	47.8	0
17Mar 04	09:00:00	3600.0	57.2	77.9	43.4	65.2	60.9	57.1	53.1	47.0	44.5	0
17Mar 04	10:00:00	3600.0	55.3	69.7	40.2	64.5	59.4	54.2	48.9	43.5	41.2	0
17Mar 04	11:00:00	3600.0	54.3	74.4	38.7	64.1	57.4	51.3	47.2	42.7	40.7	0
17Mar 04	12:00:00	3600.0	52.8	78.3	38.3	61.1	52.8	48.7	46.1	42.2	39.9	0
17Mar 04	13:00:00	3600.0	50.2	67.8	36.4	59.7	52.1	47.5	44.6	40.8	37.3	0
17Mar 04	14:00:00	3600.0	55.6	78.3	35.2	64.3	55.4	49.6	45.3	39.8	36.5	0
17Mar 04	15:00:00	3600.0	59.5	82.6	40.5	69.2	59.8	54.7	51.1	46.5	43.3	0
17Mar 04	16:00:00	3600.0	51.4	70.8	42.6	59.2	53.9	50.8	47.6	44.9	43.4	0
17Mar 04	17:00:00	3600.0	65.5	96.9	43.6	64.2	57.2	53.6	49.8	46.2	44.4	0
17Mar 04	18:00:00	3600.0	57.8	82.2	43.3	65.2	57.6	52.0	48.8	45.7	44.2	0
17Mar 04	19:00:00	328.4	54.7	68.6	43.0	65.8	58.1	50.3	45.7	44.1	43.1	0

C:\LARDAV\SLMUTIL\VICK1ST.bin Interval Data

Date	Time	Duration	Leq	Lmax	Lmin	L( 2)	L(10)	L(25)	L(50)	L(90)	L(99)	Over loads
18Mar 04	08:57:17	162.7	50.6	71.3	42.5	59.1	46.7	44.5	43.7	43.0	42.5	0
18Mar 04	09:00:00	3600.0	48.0	70.1	41.0	55.4	49.3	46.0	44.2	42.4	41.4	0
18Mar 04	10:00:00	3600.0	54.2	80.4	41.0	57.7	50.7	47.4	45.2	42.7	41.4	0
18Mar 04	11:00:00	3600.0	50.8	71.9	40.3	58.4	51.0	47.3	44.6	42.2	40.9	0
18Mar 04	12:00:00	3600.0	49.3	70.7	39.8	56.4	50.3	47.4	45.0	42.2	41.0	0
18Mar 04	13:00:00	3600.0	49.3	66.8	42.6	56.0	51.2	48.8	47.0	44.6	43.3	0
18Mar 04	14:00:00	3600.0	49.8	60.9	43.6	56.3	52.6	49.9	47.9	45.6	44.2	0
18Mar 04	15:00:00	3600.0	50.0	62.6	44.0	56.5	52.0	50.0	48.5	46.2	44.9	0
18Mar 04	16:00:00	3600.0	52.1	71.5	43.8	59.8	52.9	50.9	48.2	45.7	44.9	0
18Mar 04	17:00:00	3600.0	49.9	66.0	43.7	57.3	51.9	48.9	47.2	45.4	44.2	0
18Mar 04	18:00:00	3600.0	52.7	75.4	41.1	60.1	51.4	48.6	46.7	43.8	42.2	0
18Mar 04	19:00:00	3600.0	45.1	59.9	40.7	50.6	46.9	45.3	43.8	42.1	41.1	0
18Mar 04	20:00:00	3600.0	45.0	56.5	41.1	50.7	46.8	44.9	43.8	42.2	41.2	0
18Mar 04	21:00:00	3600.0	50.4	67.4	42.1	59.1	53.1	49.1	46.4	43.8	42.4	0
18Mar 04	22:00:00	3600.0	43.8	59.2	38.2	48.6	45.6	44.0	42.9	40.5	38.9	0
18Mar 04	23:00:00	3600.0	39.6	54.6	33.9	45.3	41.5	40.0	38.6	35.6	34.3	0
19Mar 04	00:00:00	3600.0	37.6	59.2	30.6	44.9	38.5	35.4	34.0	32.3	31.2	0
19Mar 04	01:00:00	3600.0	34.1	53.5	29.8	38.9	34.8	33.2	32.2	30.8	30.1	0
19Mar 04	02:00:00	3600.0	31.2	43.4	27.2	34.6	32.8	31.7	30.8	28.5	27.4	0
19Mar 04	03:00:00	3600.0	36.3	59.7	28.7	43.3	34.2	32.4	31.2	29.8	29.1	0
19Mar 04	04:00:00	3600.0	36.6	54.1	30.4	43.3	38.1	35.8	33.8	32.1	31.0	0
19Mar 04	05:00:00	3600.0	39.4	59.2	32.3	45.7	42.1	39.6	37.0	34.2	32.8	0
19Mar 04	06:00:00	3600.0	42.0	55.4	34.7	48.1	44.7	42.4	40.4	37.2	36.0	0
19Mar 04	07:00:00	3600.0	42.6	61.8	35.1	49.9	44.8	42.1	39.7	37.0	35.7	0
19Mar 04	08:00:00	3600.0	45.5	59.6	37.8	52.3	48.3	45.6	43.5	40.1	38.3	0
19Mar 04	09:00:00	3600.0	47.7	65.7	41.8	54.7	49.8	47.1	45.4	43.6	42.2	0
19Mar 04	10:00:00	210.8	48.1	57.2	42.8	55.8	51.4	47.4	45.3	43.4	43.0	0

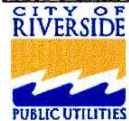
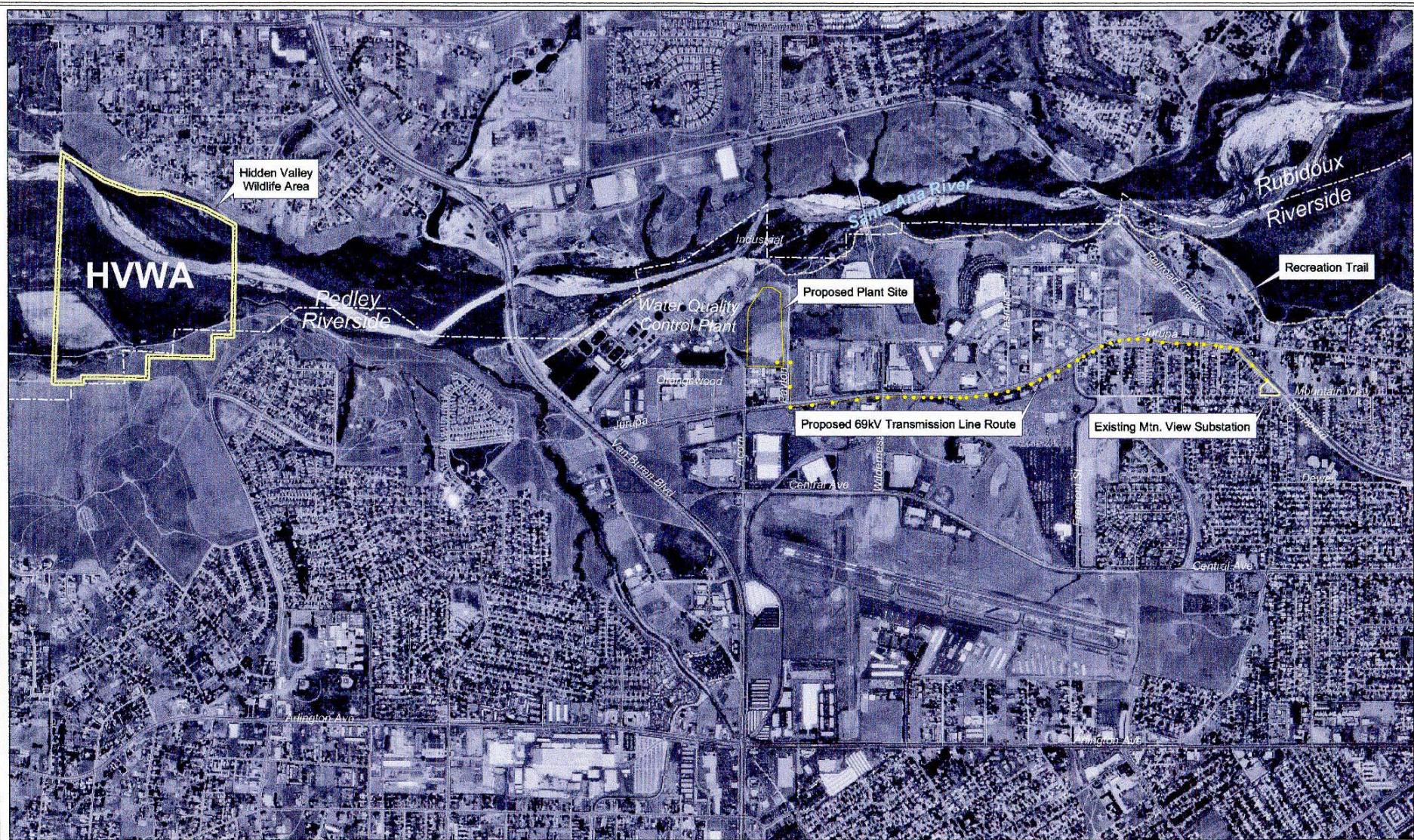
C:\LARDAV\SLMUTIL\VICK2ND.bin Interval Data

Date	Time	Duration	Leq	Lmax	Lmin	L( 2)	L(10)	L(25)	L(50)	L(90)	L(99)	Over loads
18Mar 04	08:57:00	179.8	50.3	62.4	46.8	56.6	53.2	49.9	48.6	47.2	47.0	0
18Mar 04	09:00:00	3600.0	52.1	72.2	46.3	57.2	53.5	51.2	49.5	47.7	47.0	0
18Mar 04	10:00:00	3600.0	55.5	80.6	44.8	59.7	53.8	51.4	49.4	47.1	45.5	0
18Mar 04	11:00:00	3600.0	52.5	71.2	43.3	59.0	53.9	51.4	49.1	45.9	44.4	0
18Mar 04	12:00:00	3600.0	52.5	72.7	43.3	58.6	53.9	51.2	48.8	46.4	44.7	0
18Mar 04	13:00:00	3600.0	53.5	68.6	45.8	60.2	56.5	53.8	51.4	48.2	46.7	0
18Mar 04	14:00:00	3600.0	53.4	62.6	46.8	59.0	56.1	54.0	52.1	49.3	48.0	0
18Mar 04	15:00:00	3600.0	53.5	66.7	46.6	60.0	56.1	53.8	52.0	49.3	47.8	0
18Mar 04	16:00:00	3600.0	54.5	71.1	46.5	62.4	56.4	54.1	52.0	48.5	47.2	0
18Mar 04	17:00:00	3600.0	52.4	68.2	46.2	59.6	54.9	52.4	50.3	48.0	47.0	0
18Mar 04	18:00:00	3600.0	54.6	76.0	44.7	62.2	54.3	51.7	49.5	46.4	45.1	0
18Mar 04	19:00:00	3600.0	48.0	59.1	43.2	53.9	50.2	48.3	46.6	44.8	43.7	0
18Mar 04	20:00:00	3600.0	47.6	60.4	43.5	54.1	49.4	47.5	46.3	44.6	43.8	0
18Mar 04	21:00:00	3600.0	52.7	67.6	44.6	61.5	55.6	51.8	49.0	46.2	45.1	0
18Mar 04	22:00:00	3600.0	47.5	68.3	40.9	53.0	48.7	46.7	45.3	43.1	41.7	0
18Mar 04	23:00:00	3600.0	44.2	65.6	39.4	50.8	45.4	43.5	42.4	41.0	40.0	0
19Mar 04	00:00:00	3600.0	43.4	67.7	34.1	52.3	43.2	38.3	36.6	35.1	34.1	0
19Mar 04	01:00:00	3600.0	39.5	63.1	32.7	44.9	39.0	37.2	35.6	33.7	33.0	0
19Mar 04	02:00:00	3600.0	35.3	48.8	30.7	39.0	37.7	36.3	34.5	31.8	31.0	0
19Mar 04	03:00:00	3600.0	41.9	67.2	32.1	49.4	37.6	35.6	34.3	33.0	32.1	0
19Mar 04	04:00:00	3600.0	41.7	59.7	32.8	50.9	42.8	39.6	37.2	34.9	33.4	0
19Mar 04	05:00:00	3600.0	43.6	57.4	35.5	52.1	46.5	42.4	40.6	37.5	36.1	0
19Mar 04	06:00:00	3600.0	48.2	62.4	38.9	54.9	51.7	48.7	45.7	41.2	40.0	0
19Mar 04	07:00:00	3600.0	48.2	65.7	39.6	55.8	51.5	48.0	44.5	41.6	40.2	0
19Mar 04	08:00:00	3600.0	50.0	62.5	41.6	57.2	53.1	50.2	48.0	44.1	42.2	0
19Mar 04	09:00:00	3600.0	52.0	70.8	45.3	57.6	53.7	51.5	49.7	47.4	46.0	0
19Mar 04	10:00:00	182.9	50.3	58.8	46.2	57.6	52.7	50.5	48.1	46.7	46.2	0

# **Cure Data Requests Set 3**

**Noise, Biology, Socioeconomics – Map #2**





- Recreation trail
- Proposed 69kV Transmission line
- Existing Mtn. View Substation
- Proposed Site Adjacent to 5950 Acom

## Riverside Energy Resource Center

Hidden Valley Wildlife Focus Area



Scale 1:15,940

1" = 1320 ft.

Feet

0 750 1,500



101414 Riverside Energy, Riverside Hidden Valley WA.mxd, rev1 7-09-04 jls

R:\California\Riverside\PDFs\profiles\Hidden Valley WA.pdf

Data Source: City of Riverside GIS



# **Cure Data Requests Set 3**

## **Water – Attachment 1**



Quarterly Report  
April 2004

**INFLUENT MONITORING**

Sample Date: April 5, 2004

Constituent	Composite Daily Max	Units	PQL	MDL	DNQ estimate
Arsenic	ND	µg/l	7	0.2	
Cadmium	ND	µg/l	15	0.1	
Total Chromium	10	µg/l	15	0.1	
Copper	101	µg/l	19	1.1	
Lead	DNQ	µg/l	26	0.1	4
Mercury	ND	µg/l	0.5	0.2	
Nickel	DNQ	µg/l	50	0.1	5
Silver	DNQ	µg/l	16	0.1	4
Zinc	157	µg/l	20	1.6	
Boron	0.316	mg/l		0.0001	
Chloride	97	mg/l		0.2	
Fluoride	0.58	mg/l		0.01	
Sulfate	93	mg/l		0.2	
Total Hardness	244	mg/l	5		

**INFLUENT MONITORING**

Sample Date: April 5, 2004

Constituent	Composite Daily Max	Units	PQL	MDL	DNQ estimate
Cyanide, Free	ND	µg/l	50	4	

**EFFLUENT MONITORING**

Sample Date: April 5, 2004

Constituent	Composite Daily Max	Units	PQL	MDL	DNQ estimate
Bicarbonate	175	mg/l			
Carbonate	0	mg/l			
Boron	0.31	mg/l		0.0001	
Calcium	71.6	mg/l	0.1	0.055	
Chloride	110	mg/l	5		
Fluoride	0.74	mg/l		0.01	
Magnesium	13.8	mg/l		0.008	
Manganese	0.024	mg/l	0.02	0.0001	
Sodium	110	mg/l	0.1	0.03	
Sulfate	104	mg/l	5		
Total Hardness	235	mg/l	5		
Selenium	ND	ug/l	14	0.4	
Arsenic	ND	µg/l	7.5	0.2	
Barium	13	µg/l	20	1	
Cobalt	ND	µg/l	1	0.2	
Iron	82	µg/l	100	3.4	
Nickel	5	µg/l	50	1	
Zinc	28	µg/l	20	1.6	
Total Organic Carbon	12.9	mg/l		0.3	

Sample Date: April 5, 2004

Page 2 of 2